



## Results from Instrumentation of WAY30 Perpetual Pavement

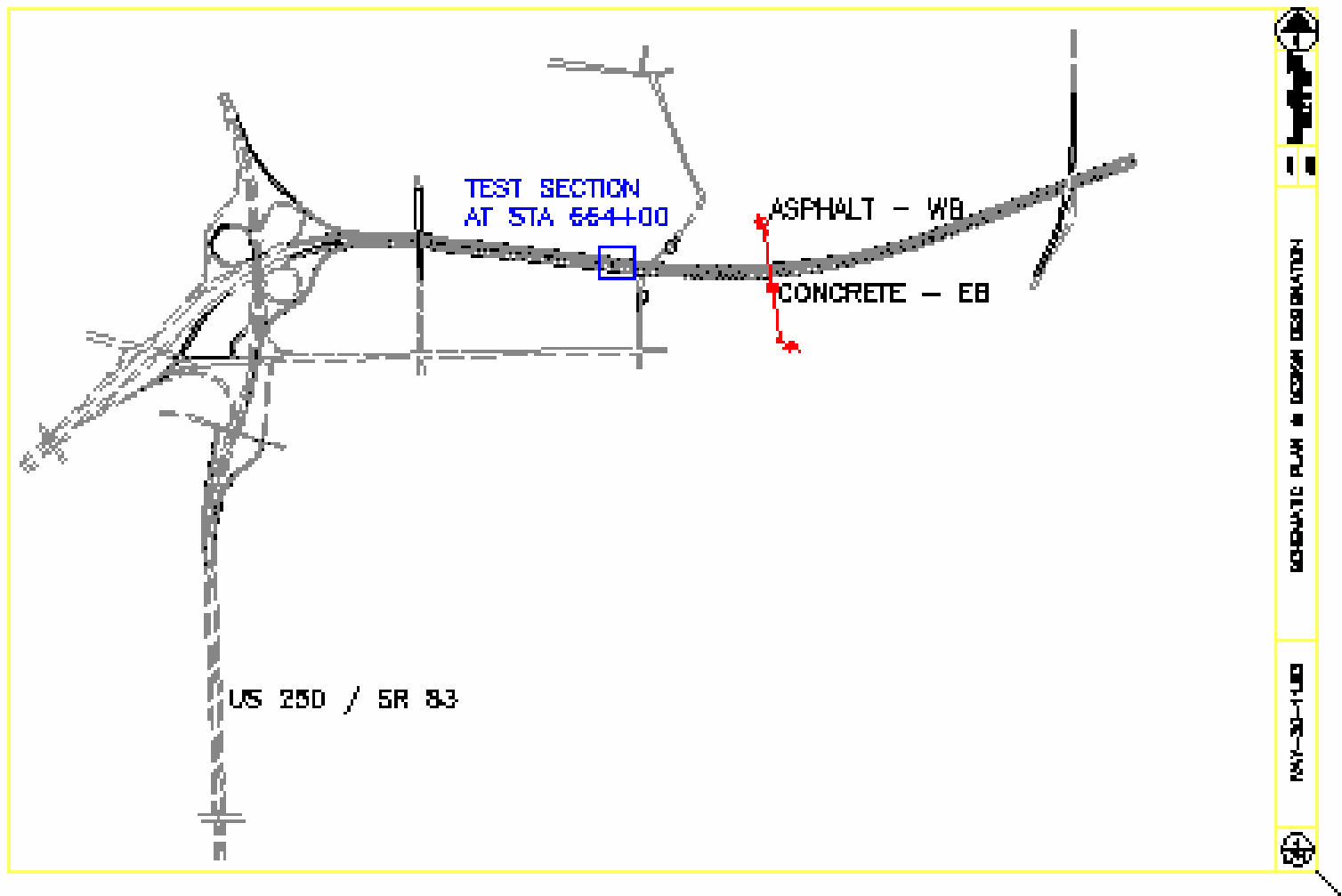
September 12, 2007  
Flexible Pavements of Ohio  
Cleveland

Shad Sargand, Russ Professor  
Ludwig Figueroa, Professor  
Department of Civil Engineering  
Ohio University



# WAY-30 Instrumentation

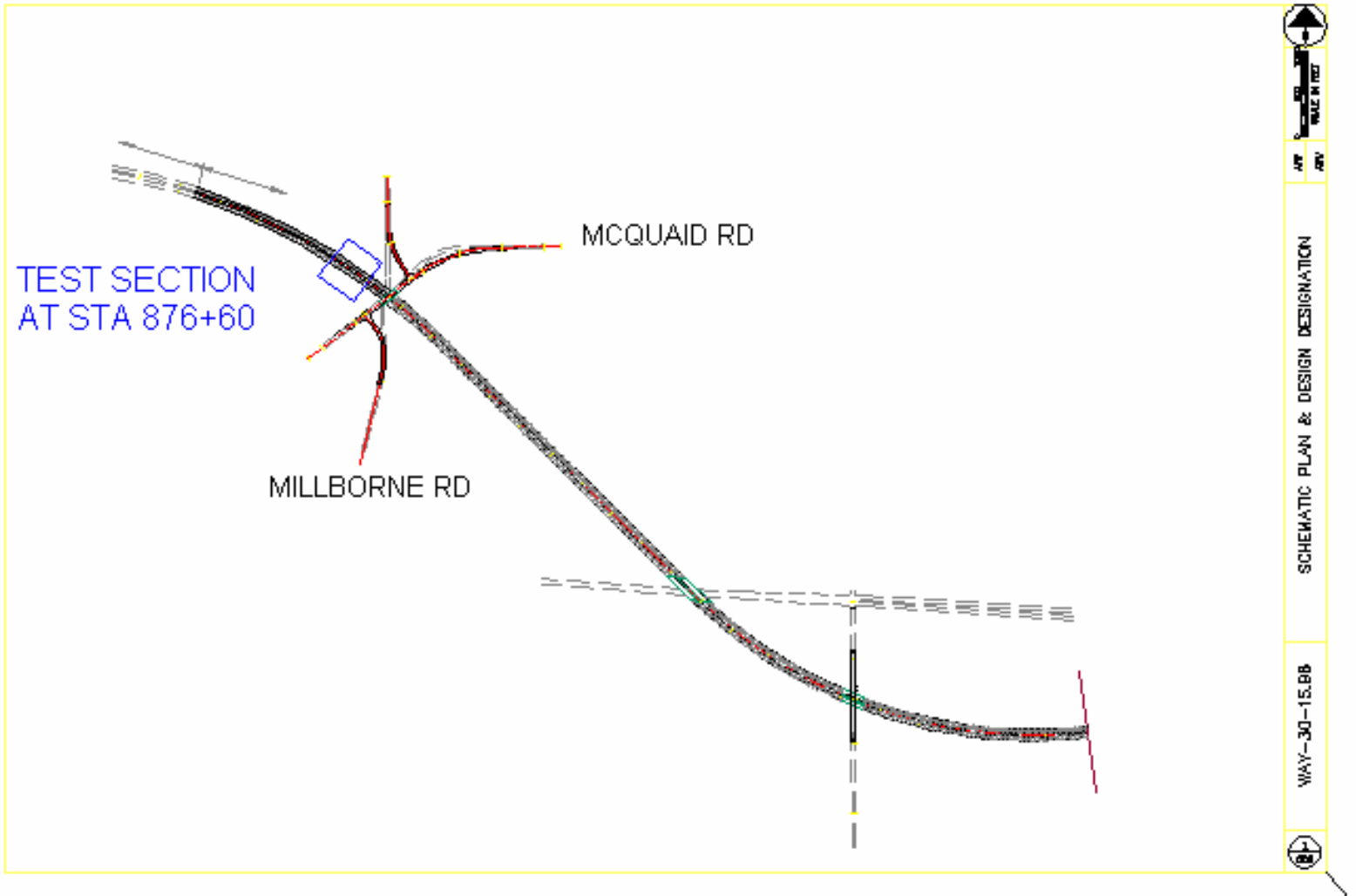
## US 30 Bypass of Wooster, Ohio



# Test Section at Geyer's Chapel



# WAY-30 Instrumentation





# Test Section at McQuaid Road



# Instrumentation Plan

- ORITE's instrumentation plan is to monitor environmental and response parameters in each pavement type.
- Instruments will be purchased and calibrated, then installed during the construction process
- Environmental parameters to be monitored in only one section of each pavement type.
- Dynamic load responses will be collected in duplicate sections of both pavements

# Instrumentation

## Asphalt Concrete Test Sections

### Environmental Parameters

| <u>MEASUREMENT</u> | <u>LAYERS</u>               | <u>MANUFACTURER</u>        | <u>SENSOR</u>  |
|--------------------|-----------------------------|----------------------------|----------------|
| Temperature        | Pavement, Base and Subgrade | Measurement Research Corp. | MRC Thermistor |
| Moisture           | Base and Subgrade           | Campbell Scientific, Inc.  | TDR Probes     |

Automatic weather station installed to collect data related to air temperature, precipitation (rain and snow), wind speed and direction, relative humidity, and incoming solar radiation.

# Instrumentation

## Asphalt Concrete Test Sections

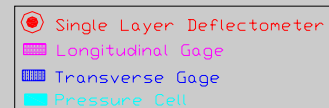
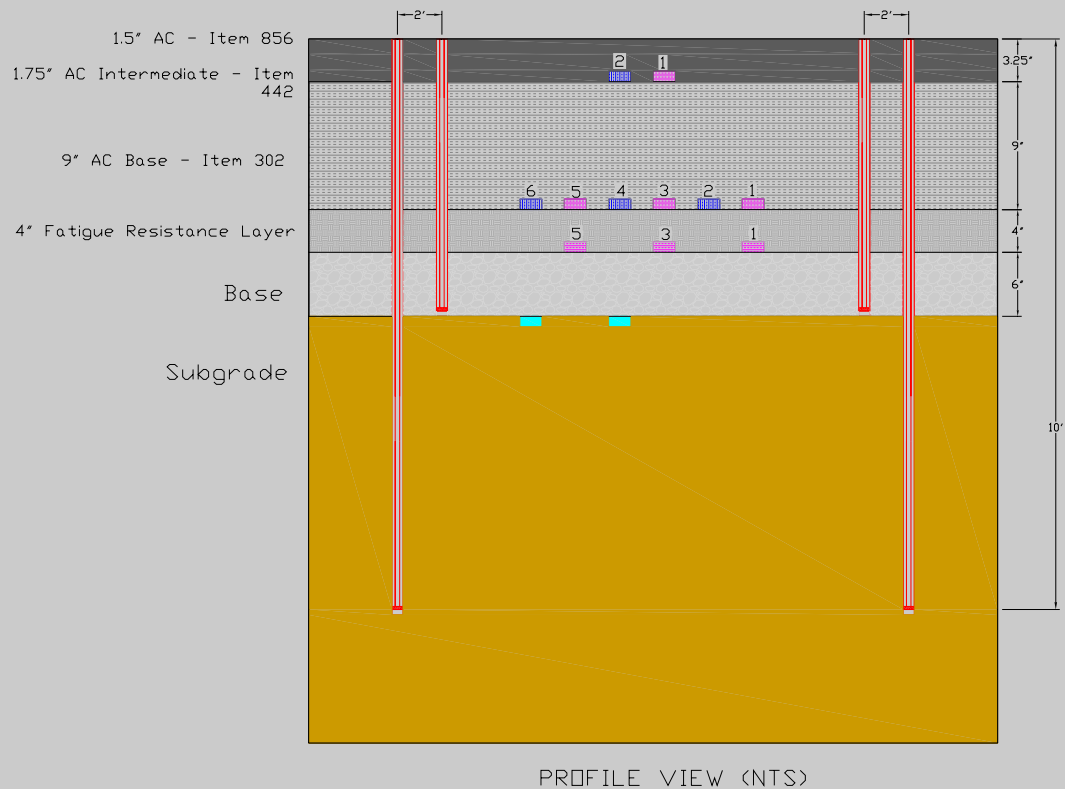
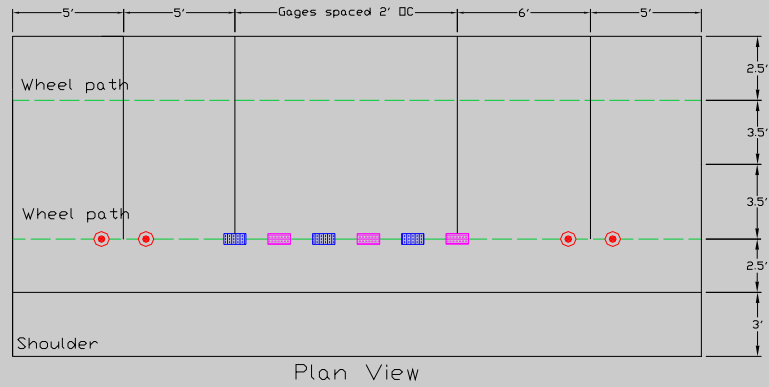
### Response Parameters

| <u>MEASUREMENT</u> | <u>PARAMETERS</u>                   | <u>MANUFACTURER</u> | <u>SENSOR</u>  |
|--------------------|-------------------------------------|---------------------|--|
| Displacement       | Load Response and Seasonal Response | Macro Sensors       | Macro Sensors LVDTs<br>(Linear Variable Displacement Transducer) |
| Pressure           | Load Response and Seasonal Response | Geokon Inc.         | Geokon 3500 Pressure Cell  |
| Strain             | Longitudinal and Transverse Strain  | Dynatest            | Dynatest PAST II Strain Transducer                               |



# AC Section A

A  
C  
S  
E  
C  
T  
I  
O  
N



AC STN 876 SECTION A LABELING

# Instrumentation

- Shallow LVDTs will monitor displacement above the subgrade
- Deep LVDTs will monitor the total displacement in the pavement system
- This combination of LVDTs help distinguish the movement between the subgrade and base.
- Two pressure cells will measure the vertical pressure applied to the base as a measure of support in each section.
- Strain gauges are placed in the wheel path of varying layers to measure transverse and longitudinal strain during controlled vehicle testing.

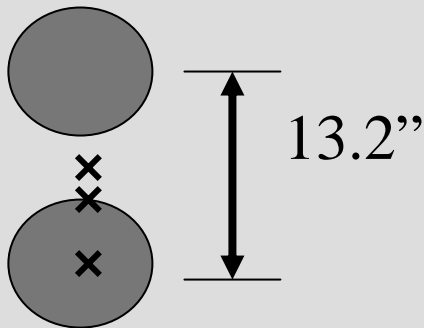
# Controlled Vehicle Load (CVL) Testing

- December 2005
- July 2006
- Single axle and tandem axle loads
- Speeds 5 mph, 25 mph (July) or 30 mph (Dec), 45 mph, and 55 mph (July) or 60 mph (Dec)

# CVL Load Configurations

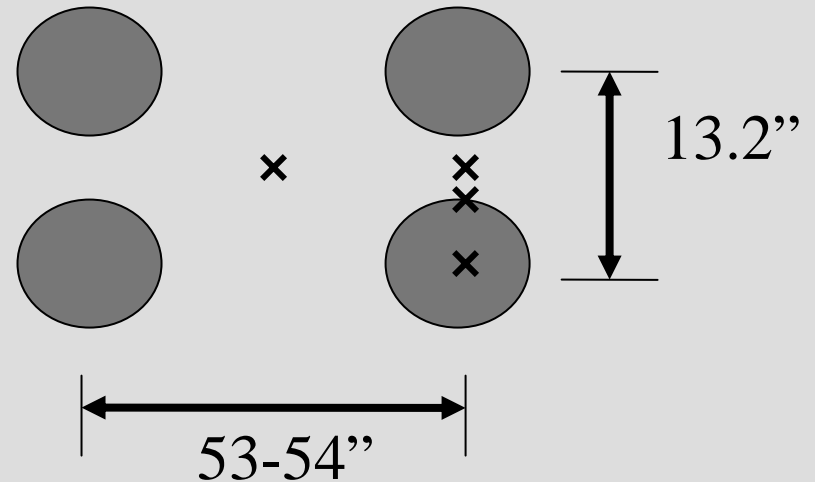
- **Single Axle**

- 28.2 kip (December) and 20.35 kip (July)
- Tire Pressure = 100 psi



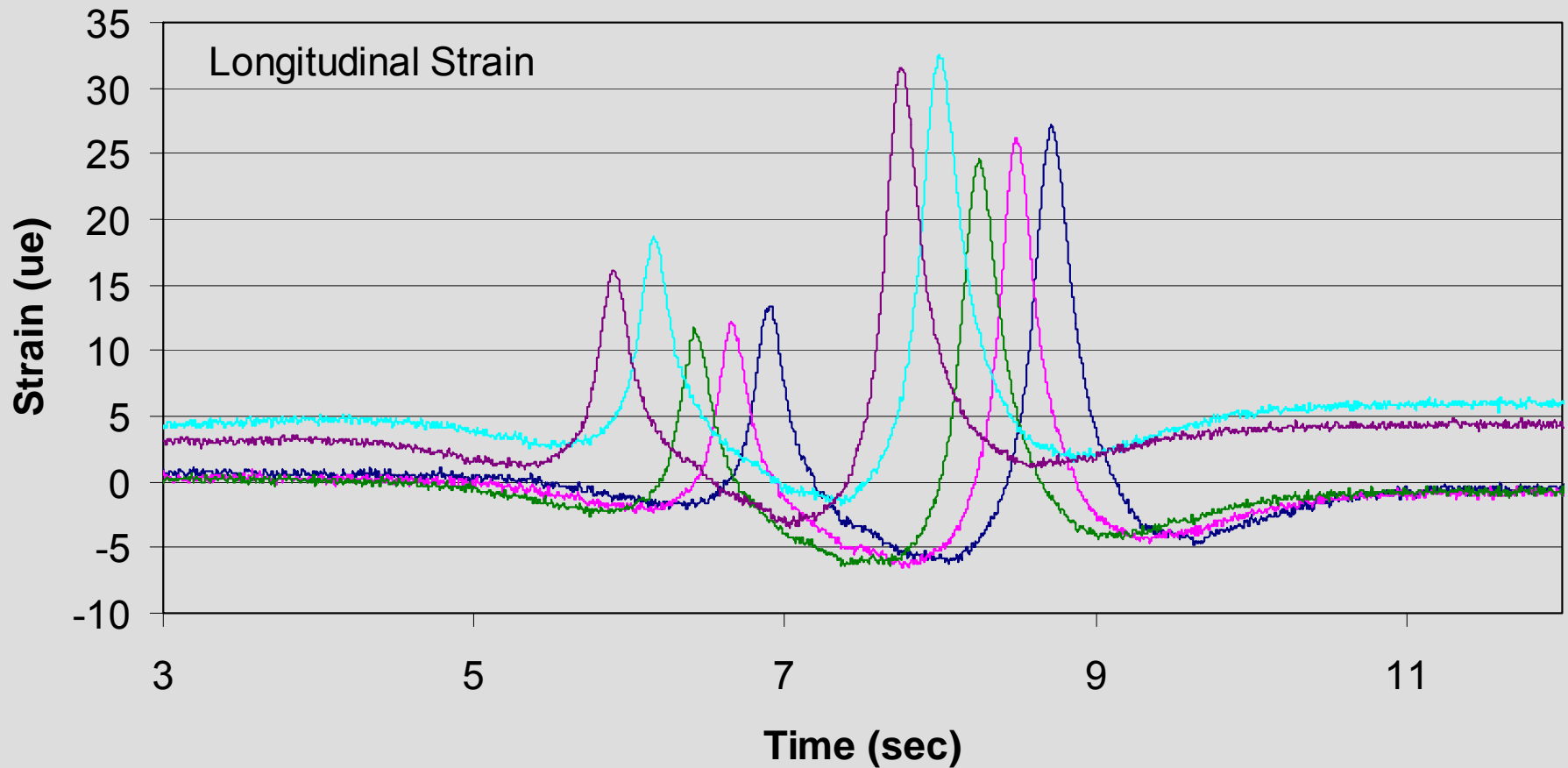
- **Tandem Axle**

- Loads: 40.15 kip (December) and 34.55 kip (July)
- Tire Pressure = 100 psi



# WAY-30 FRL Strain Response Dec. 2005

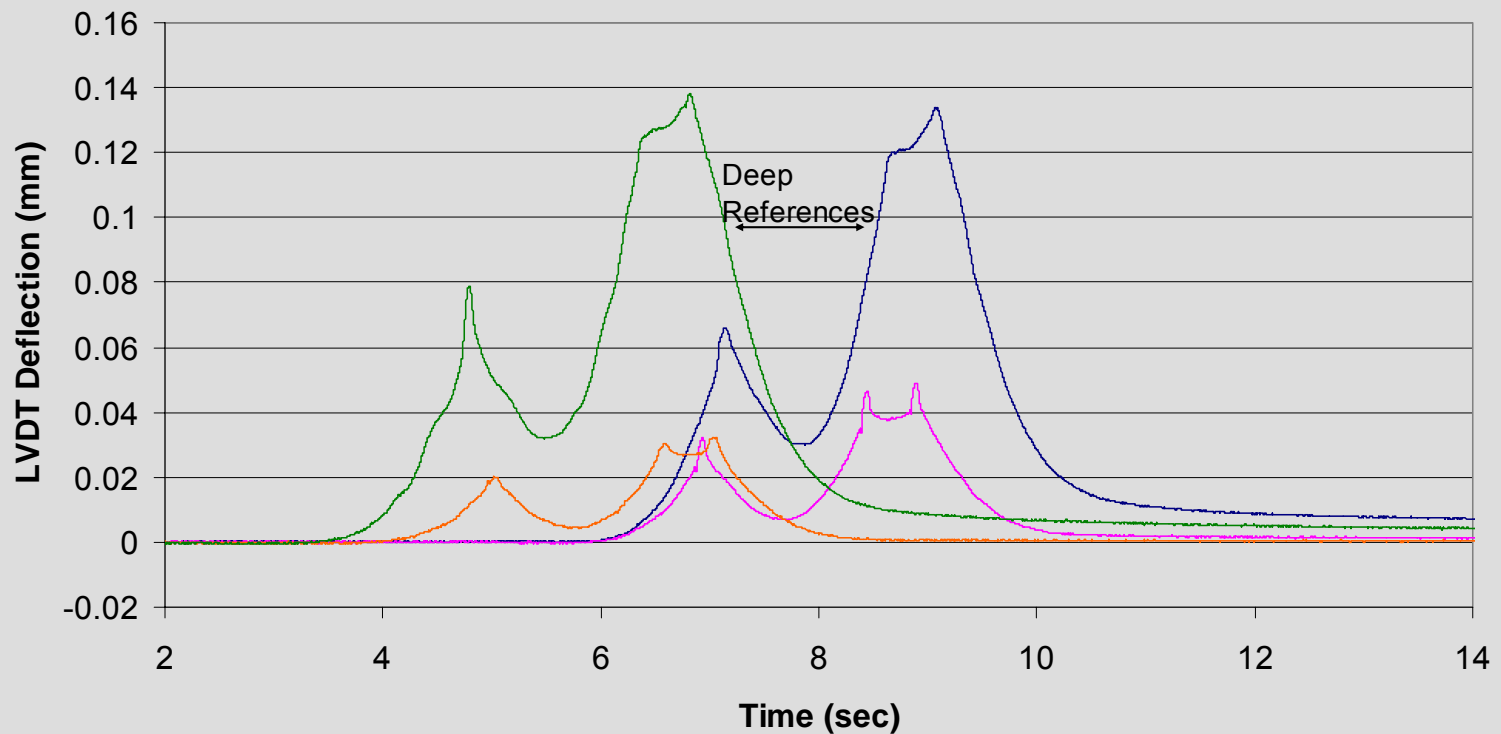
5 mph Test: ODOT 28.2 Kip Single Axle Truck





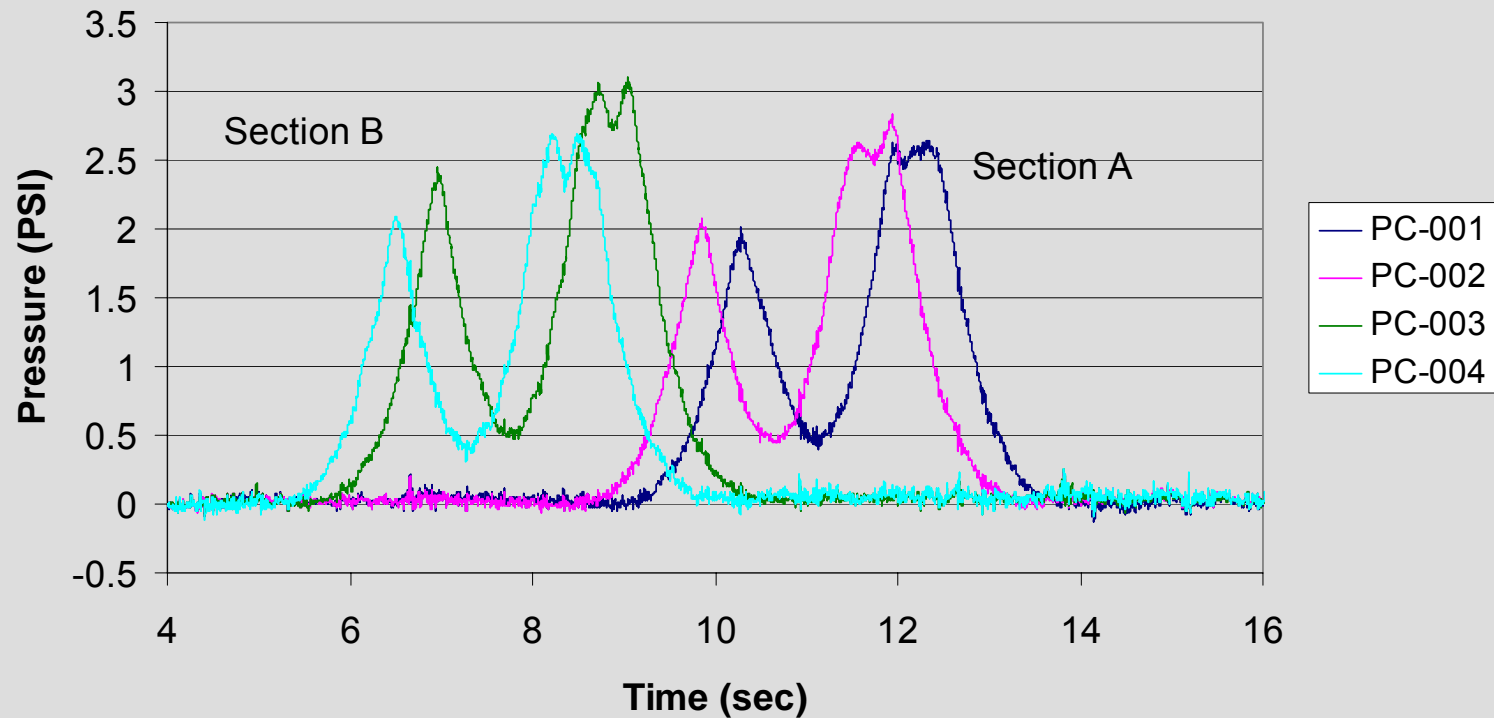
# WAY-30 LVDT Response Dec. 2005

5 mph Test: ODOT 40 Kip Tandem Axle Truck



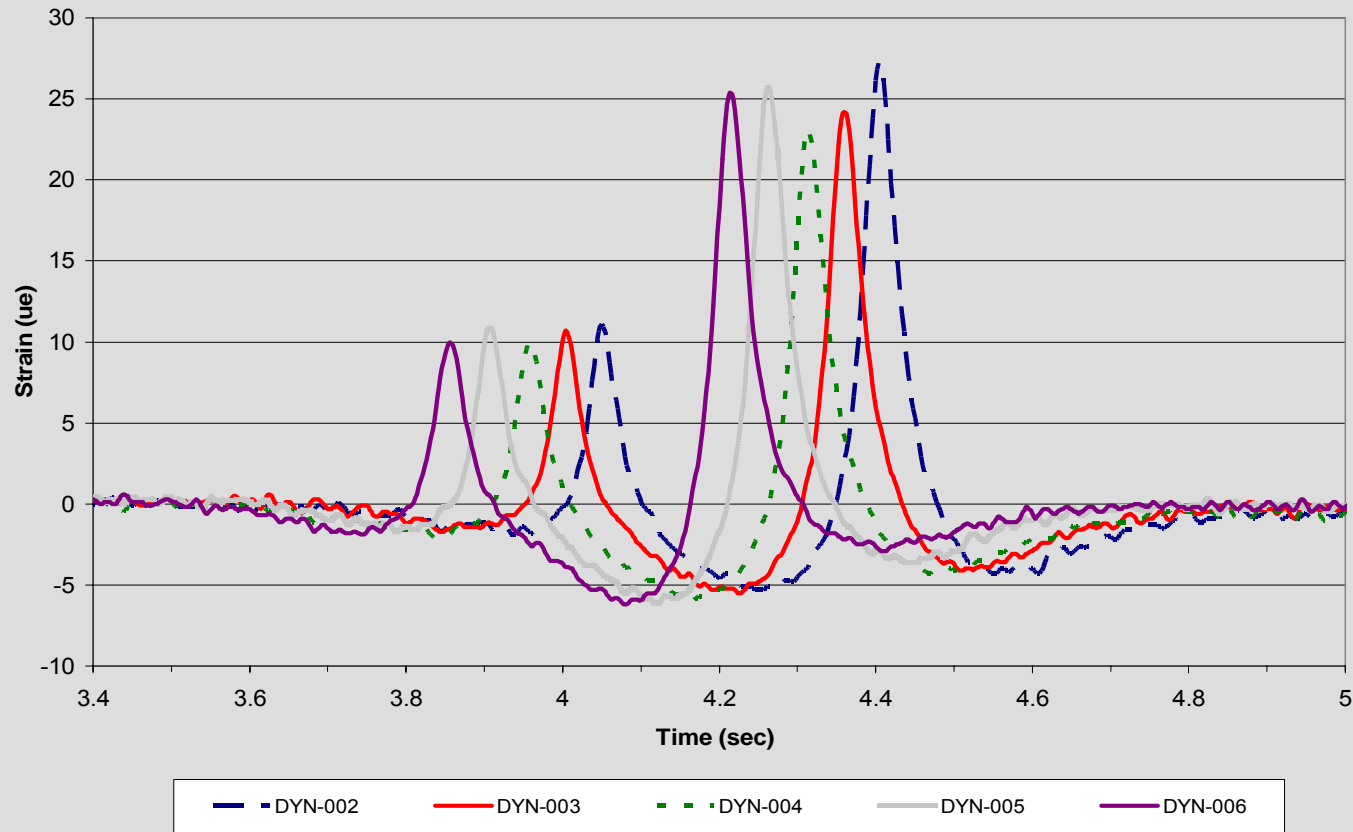
# WAY-30 Pressure Cell Readings Dec. 2005

5 mph Test: ODOT 40 Kip Tandem Axle Truck



# Longitudinal Strain – Sect. 664 (AC2-390182) FRL Layer Dec. 2005

30 mph Test: ODOT 28.2 Kip Single Axle Truck



# Maximum Tensile Strains in Fatigue Resistant Layer Test Section 664 (AC2 - 390182) Dec. 2005

|                | Max.Tensile Strain, $\mu\epsilon$ |         |                  |         |
|----------------|-----------------------------------|---------|------------------|---------|
| Speed<br>(mph) | 28.5k Single Axle                 |         | 40 k Tandem Axle |         |
|                | Maximum                           | Average | Maximum          | Average |
| 5              | 32.6                              | 29.0    | 19.5             | 17.1    |
| 30             | 27.2                              | 23.9    | 19.6             | 17.7    |
| 45             | 27.4                              | 25.1    | 21.5             | 17.4    |
| 60             | 27.7                              | 24.9    | 19.9             | 18.3    |

Note: 1 mph = 1.6 km/h  
1 kip = 4.448 kN

# Maximum Tensile Strains in Fatigue Resistant Layer Test Section 876A (AC1 - 390181) Dec. 2005

|                | Max.Tensile Strain, $\mu\epsilon$ |         |                  |         |
|----------------|-----------------------------------|---------|------------------|---------|
| Speed<br>(mph) | 28.5k Single Axle                 |         | 40 k Tandem Axle |         |
|                | Maximum                           | Average | Maximum          | Average |
| 5              | 23.1                              | 20.5    | 15.3             | 13.9    |
| 30             | 18.8                              | 16.8    | 14.9             | 13.0    |
| 45             | 18.6                              | 15.5    | 15.4             | 14.3    |
| 60             | 18.5                              | 16.8    | 15.0             | 12.0    |

Note: 1 mph = 1.6 km/h  
1 kip = 4.448 kN



# Maximum Tensile Strains in Fatigue Resistant Layer Test Section 876A (AC1 - 390181) Dec. 2005

|                | Max.Tensile Strain, $\mu\epsilon$ |         |                    |         |
|----------------|-----------------------------------|---------|--------------------|---------|
| Speed<br>(mph) | 17.5k Single Axle                 |         | 28.5 k Tandem Axle |         |
|                | Maximum                           | Average | Maximum            | Average |
| 5              | 14.9                              | 12.8    | 12.7               | 11.4    |
| 30             | 12.9                              | 11.4    | 11.1               | 10.2    |
| 45             | 11.5                              | 10.8    | 10.2               | 9.0     |
| 60             | 11.8                              | 10.2    | 10.3               | 9.7     |

Note: 1 mph = 1.6 km/h  
1 kip = 4.448 kN

# Maximum Tensile Strain in the Intermediate Layer Dec. 2005

8 km/h (5 mph)

| Test<br>Section | Maximum Tensile Strain, $\mu\epsilon$ |         |                 |         |
|-----------------|---------------------------------------|---------|-----------------|---------|
|                 | 28.5k Single Axle                     |         | 40k Tandem Axle |         |
|                 | Max                                   | Average | Max             | Average |
| 664             | 19.9                                  | 17.8    | 12.1            | 10.9    |
| 876A            | 12.9                                  | 11.8    | 8.2             | 7.7     |

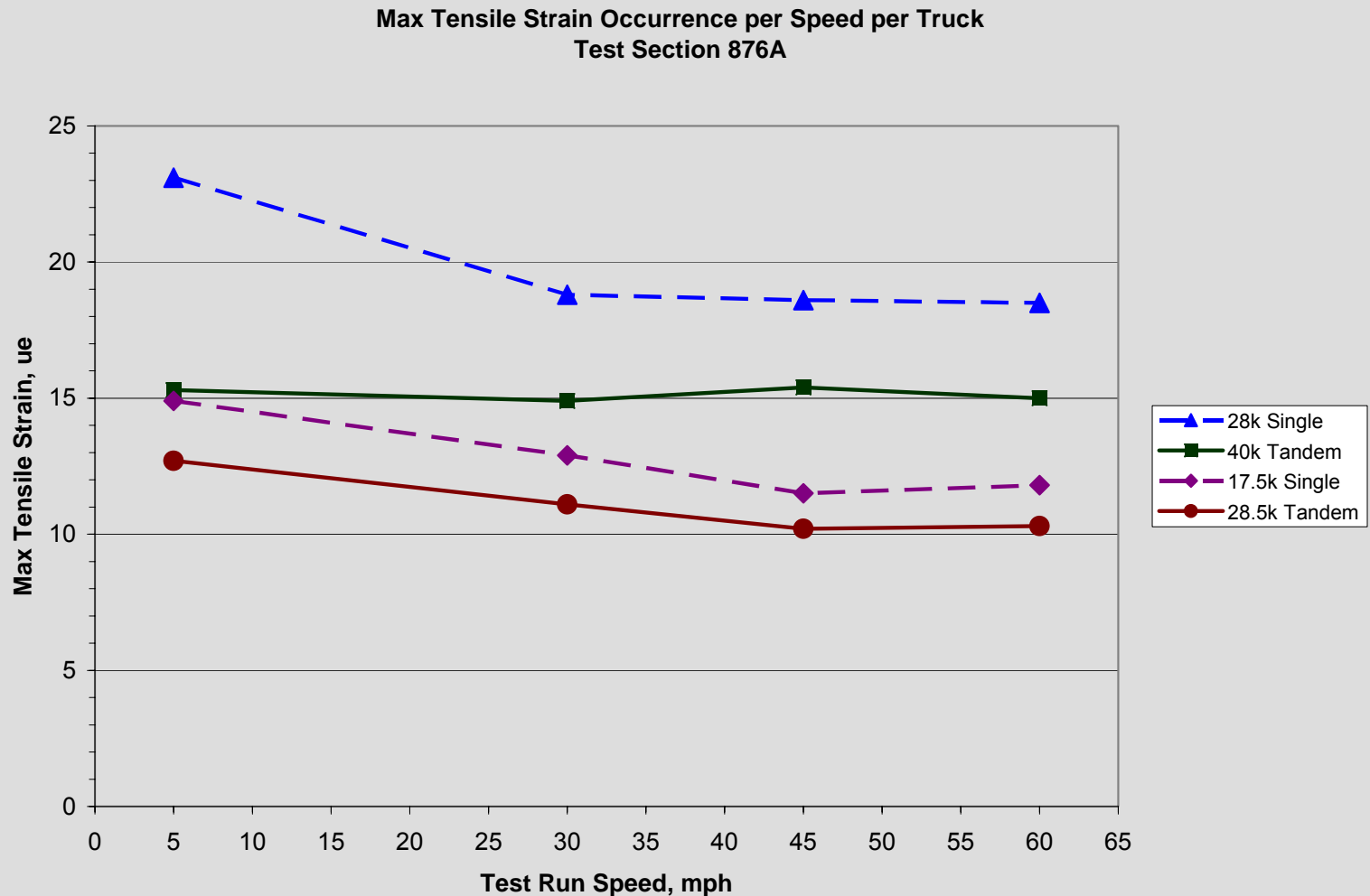
# Maximum Transverse Strains in the Intermediate Layer Dec. 2005

8 km/h (5 mph)

| Test Section | Maximum Transverse Strain, $\mu\epsilon$ |         |                 |         |
|--------------|--|---------|-----------------|---------|
|              | 28.5k Single Axle                        |         | 40k Tandem Axle |         |
|              | Max                                      | Average | Max             | Average |
| 664          | 14.2                                     | 12.4    | 11.4            | 10.9    |
| 876A         | 8.8                                      | 8.3     | 7.7             | 7.3     |

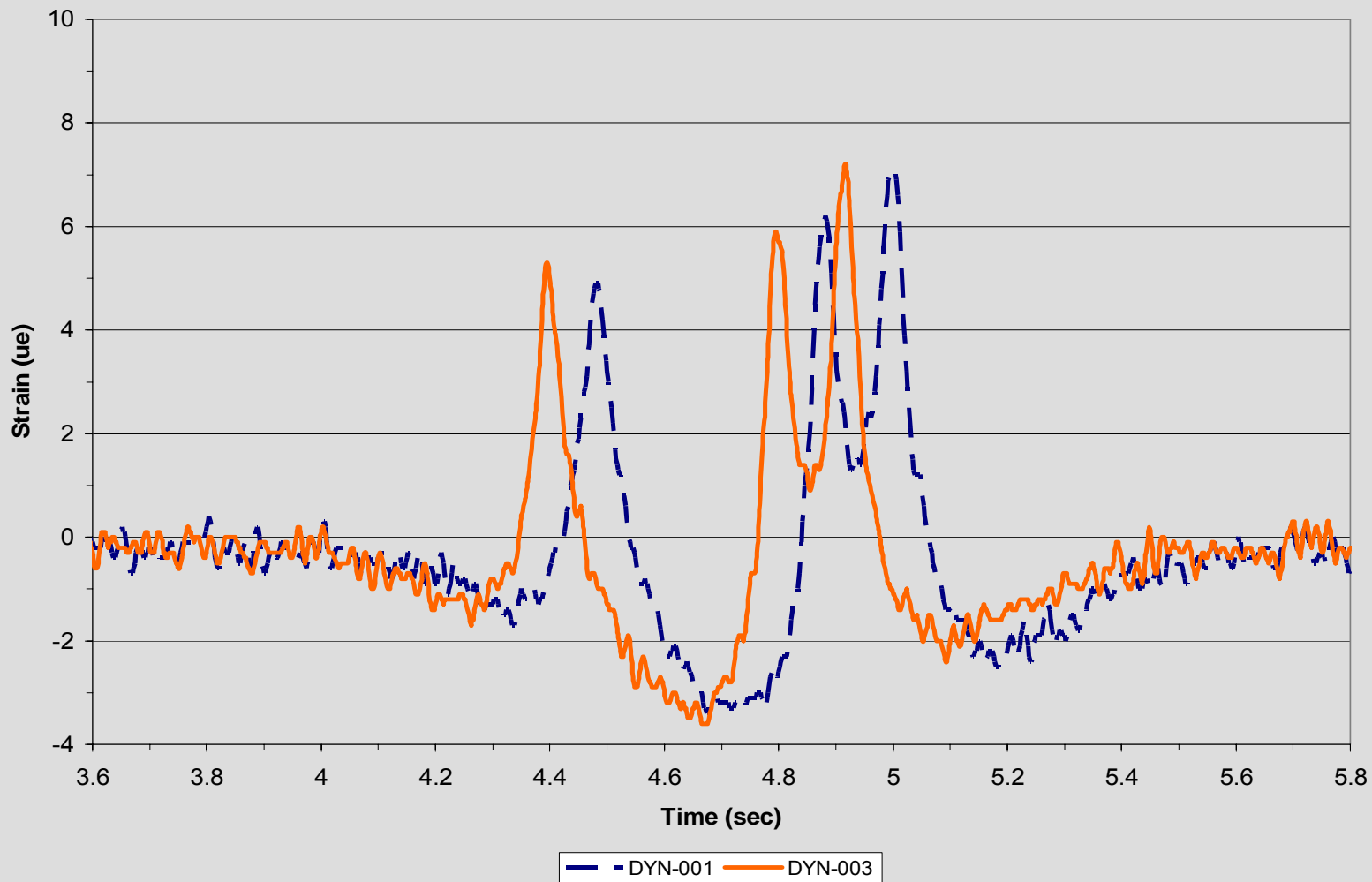
# Maximum Tensile Strain Variation vs. Speed and Axle Type Dec. 2005

## Section 876A (AC1 - 390181)



# Longitudinal Strain: Section 876A (AC1-390181) – FRL Layer Dec. 2005

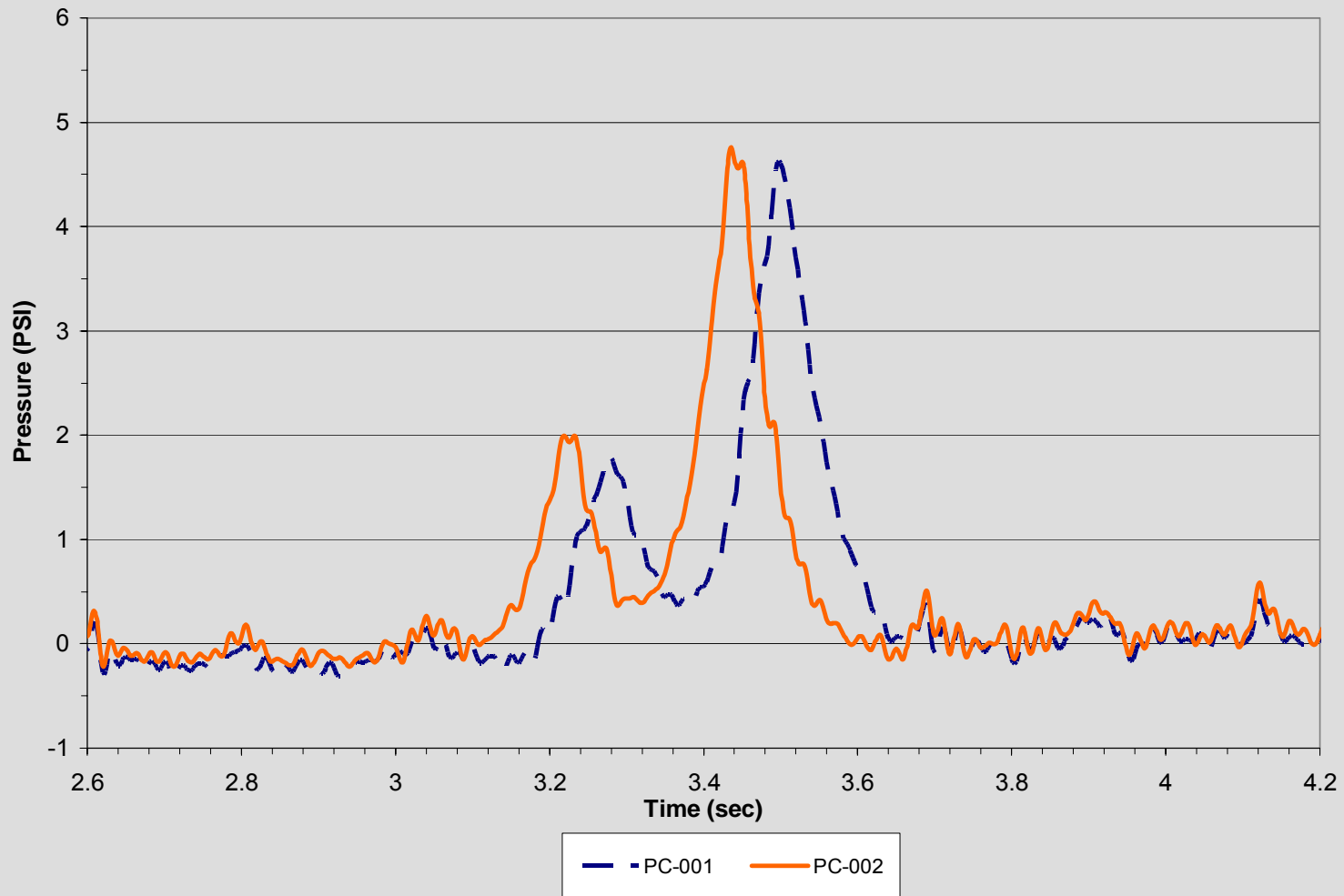
30 mph Test: ODOT 40 Kip Tandem Axle Truck





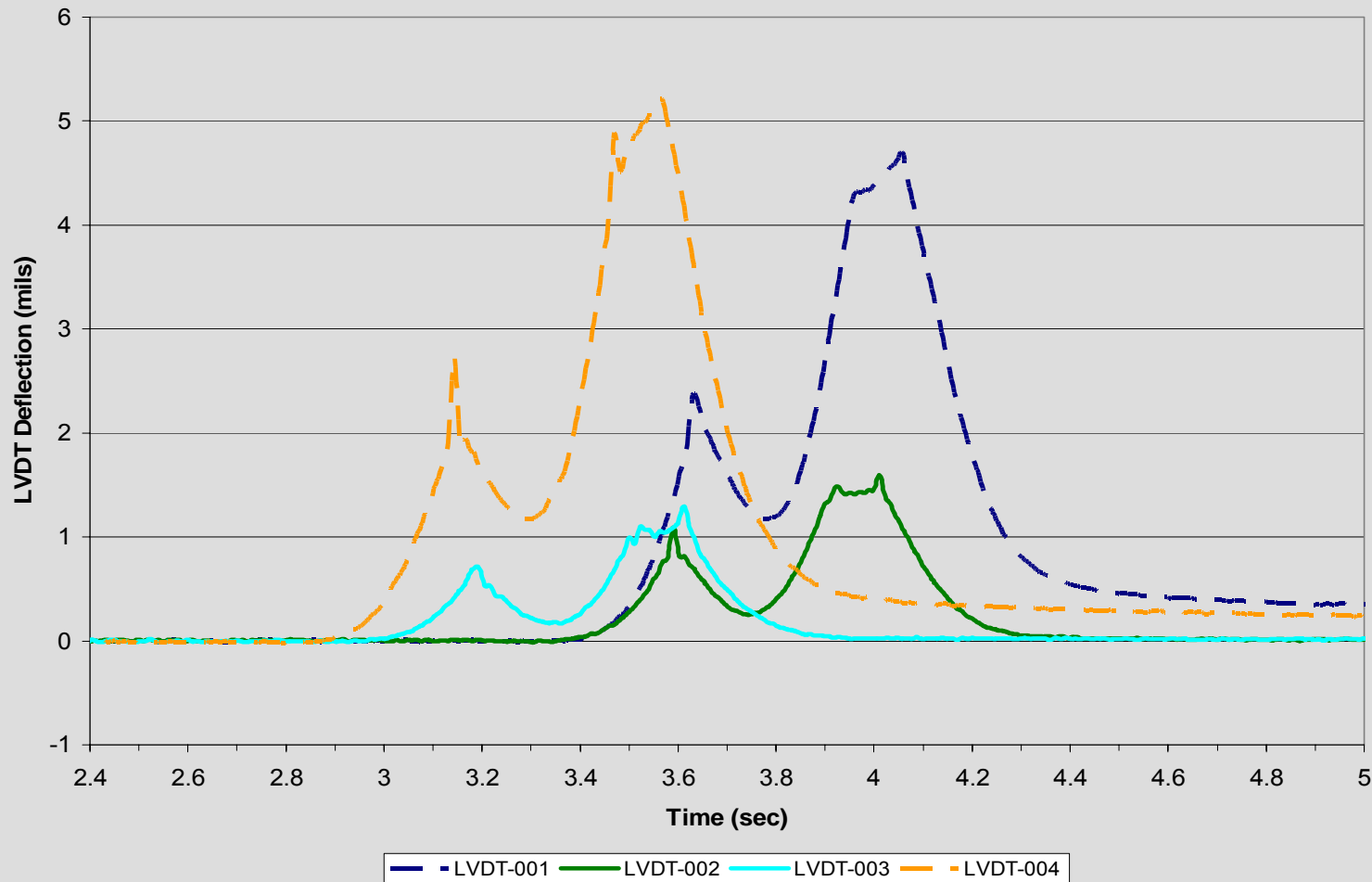
# Pressure Readings: Section 664 (AC2-390182) Dec. 2005

(28 kip Single Axle Load, 45 mph)



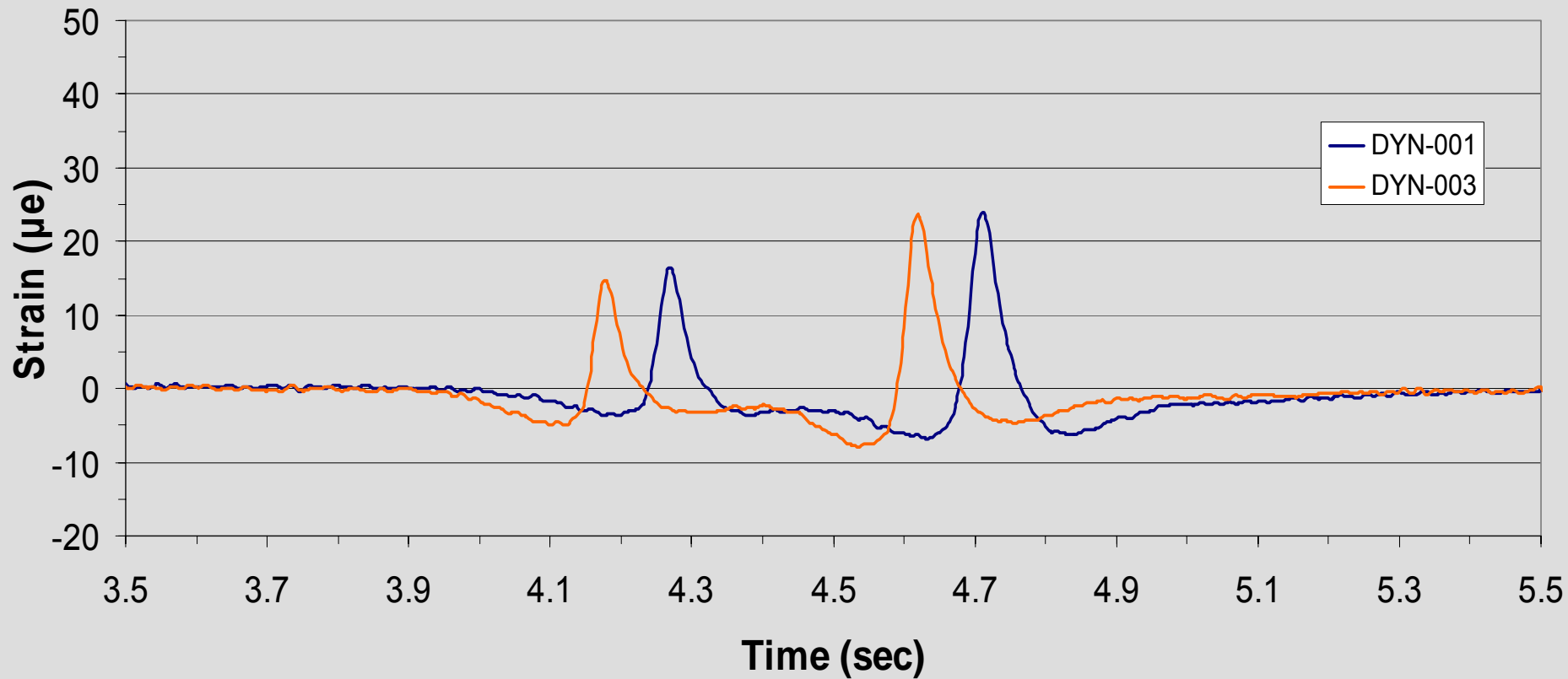
# LVDT Deflections: Section 664 (AC2-390182) Dec. 2005

40 kip. Tandem Axle Load – 30 mph



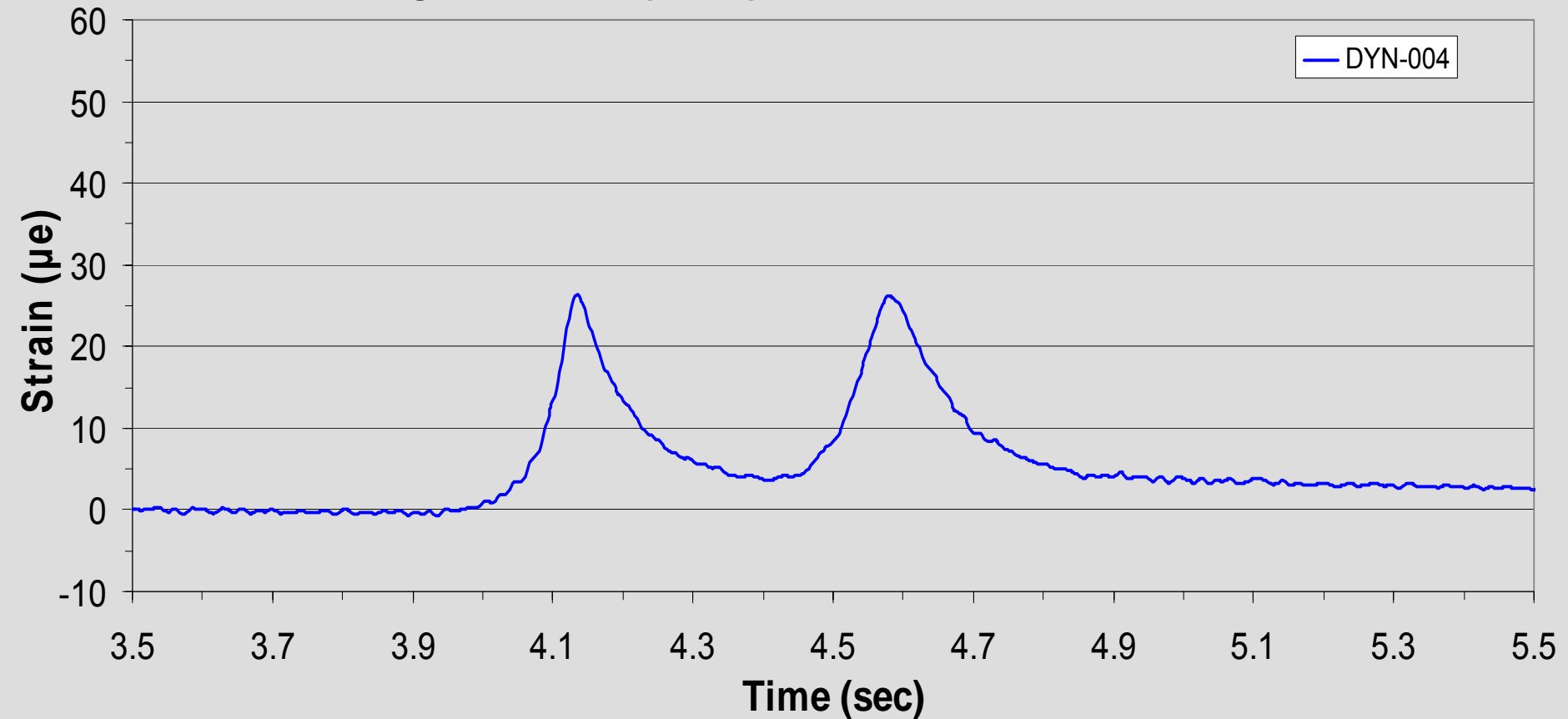
# AC CVL Test, July 2006

Longitudinal Strain in Intermediate Layer --  
Single Axle 20.5 kip 25 mph- AC 876A - Run 3 07/18/2006



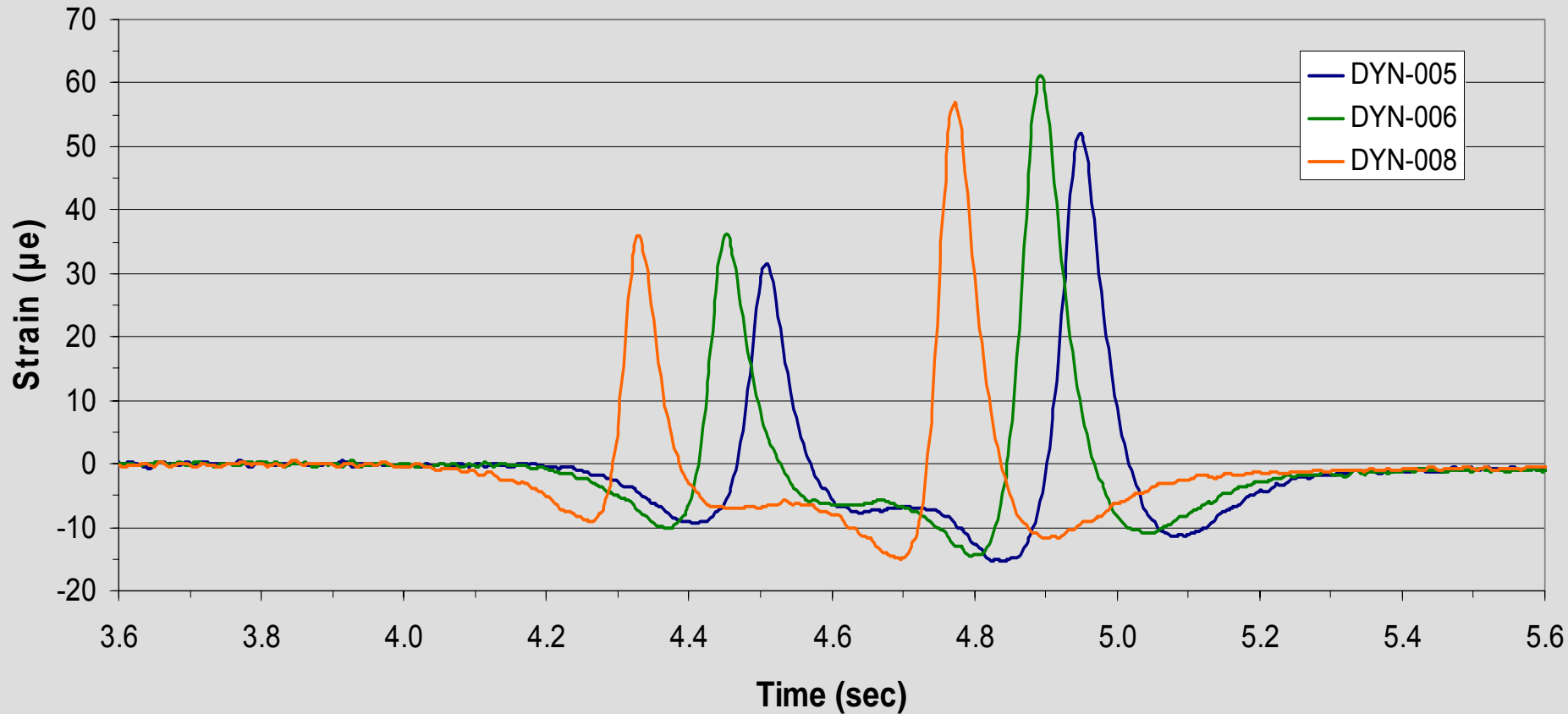
# AC CVL Test, July 2006

Transverse Strain in Intermediate Layer --  
Single Axle 20.5 kip 25 mph- AC 876A - Run 3 07/18/2006



# AC CVL Test, July 2006

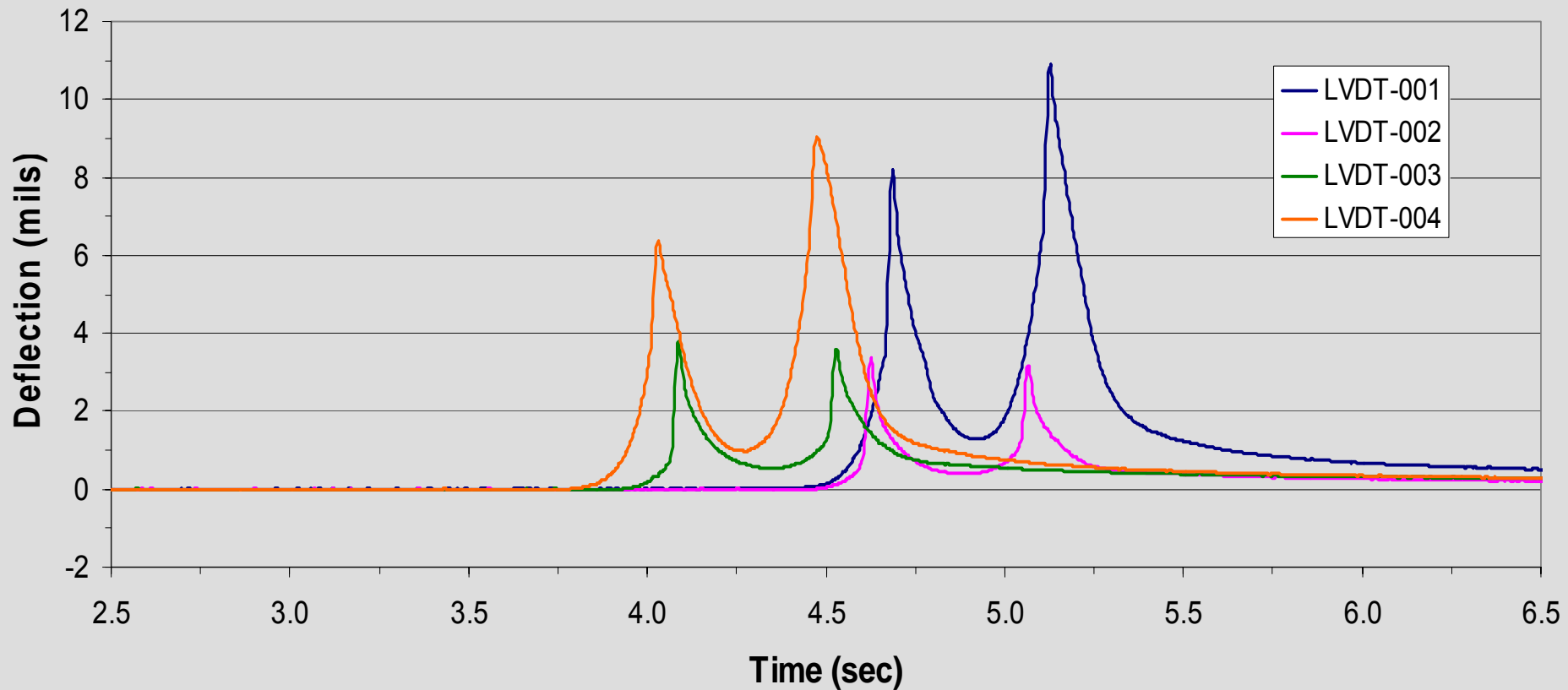
Longitudinal Strain in Fatigue Resistance Layer -- Single Axle 20.5 kip 25 mph-  
AC 876A - Run 3 07/18/2006





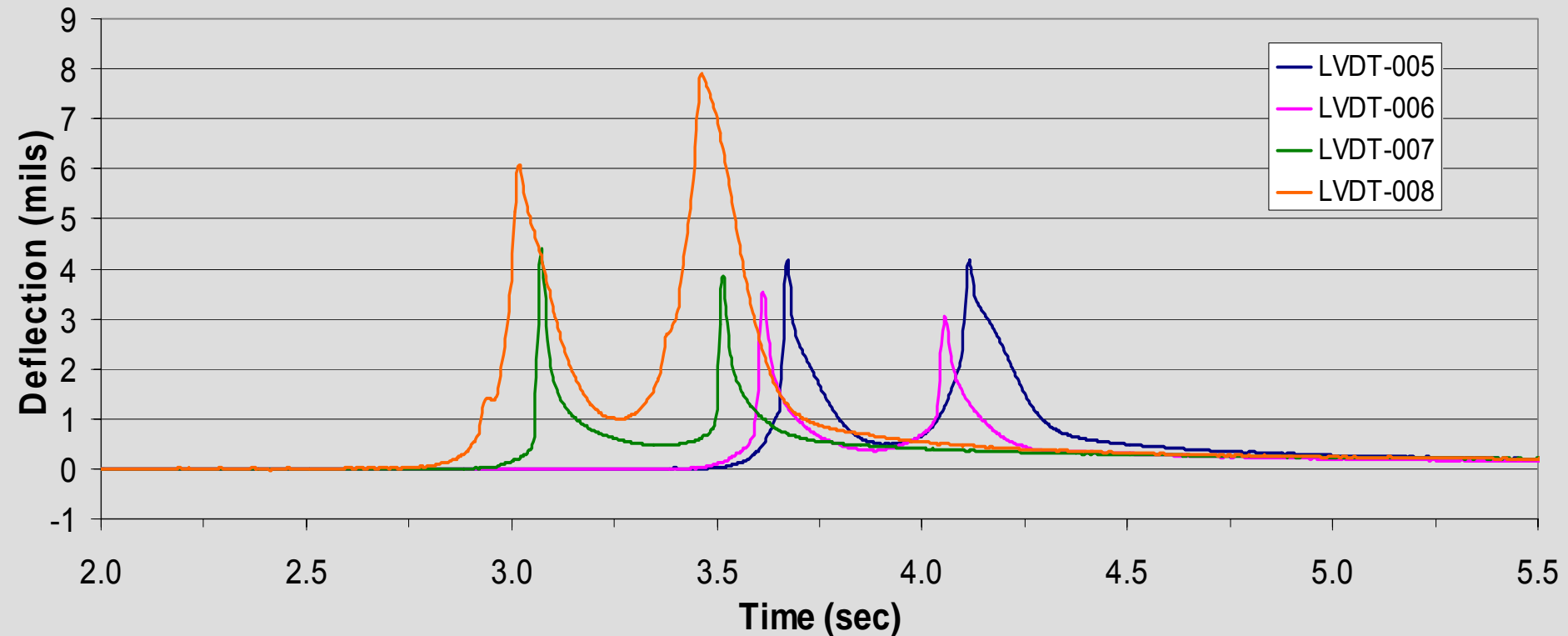
# AC CVL Test, July 2006

LVDT Deflections Single Axle 20.5 kip 25 mph  
AC 876A Run 3 July 18, 2006



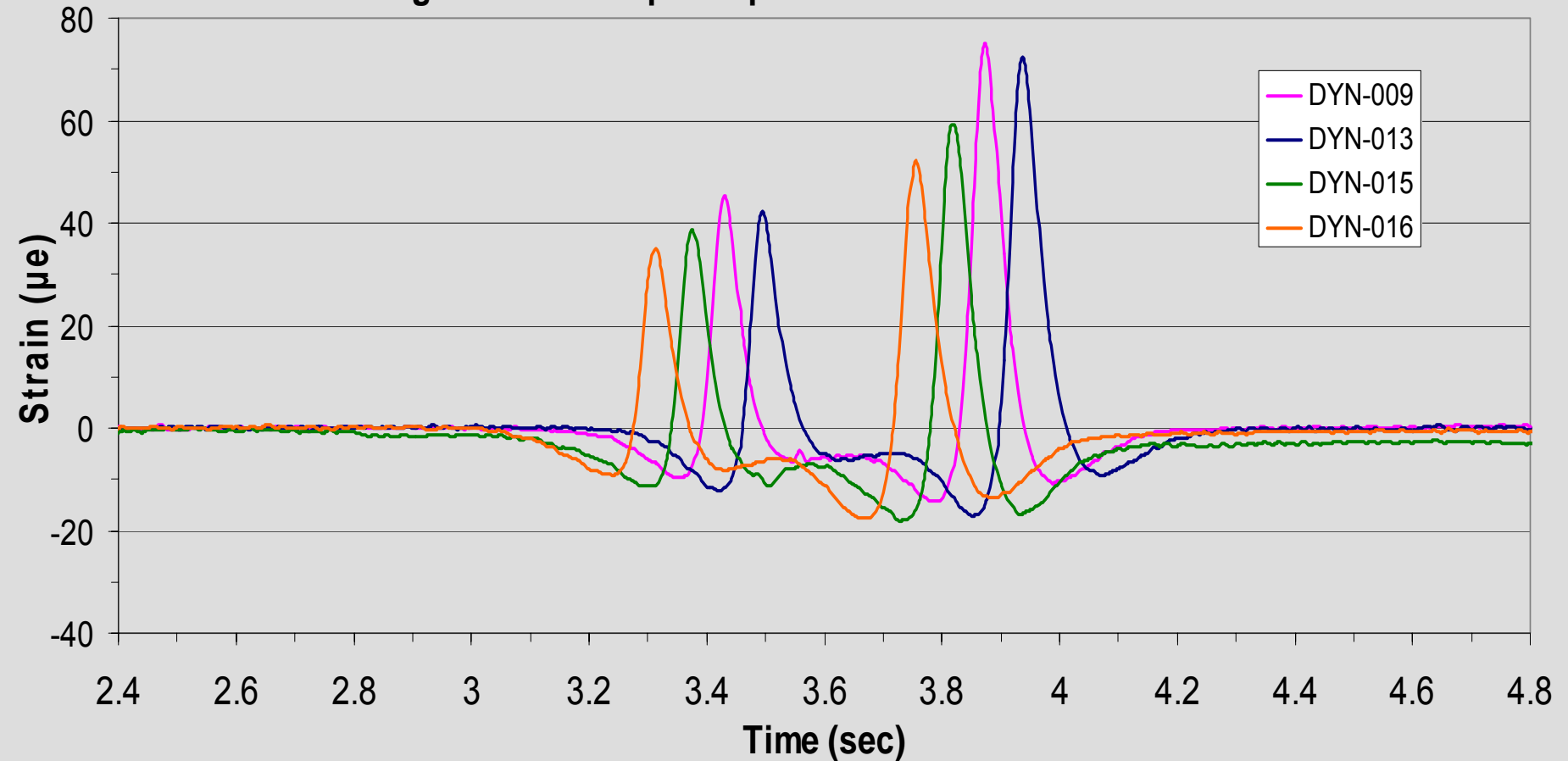
# AC CVL Test, July 2006

LVDT Deflections Single Axle 20.5 kip 25 mph  
AC 876B Run 3 July 18, 2006



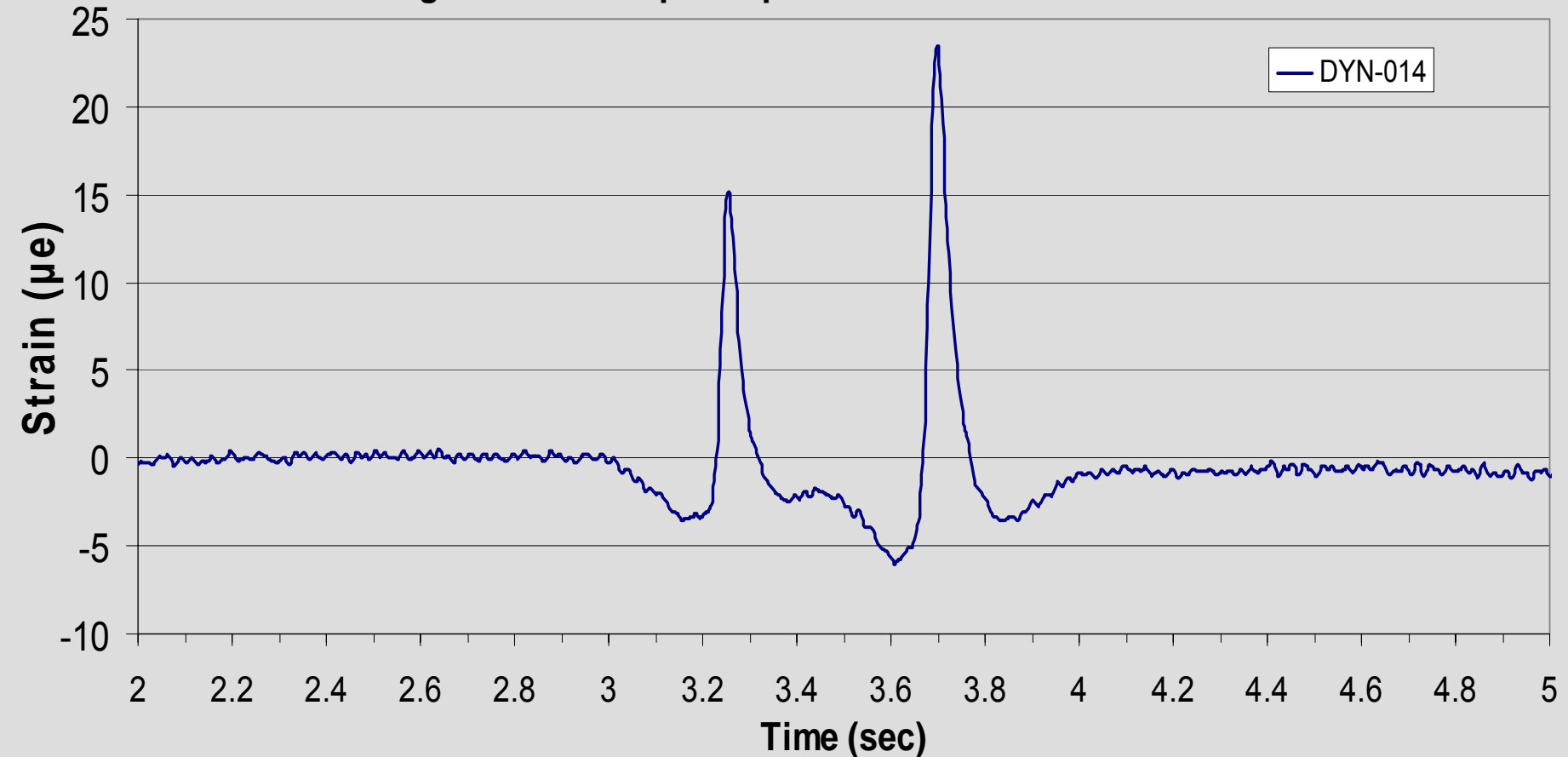
# AC CVL Test, July 2006

Longitudinal Strain in Fatigue Resistance Layer --  
Single Axle 20.5 kip 25 mph- AC 876B - Run 3 07/18/2006



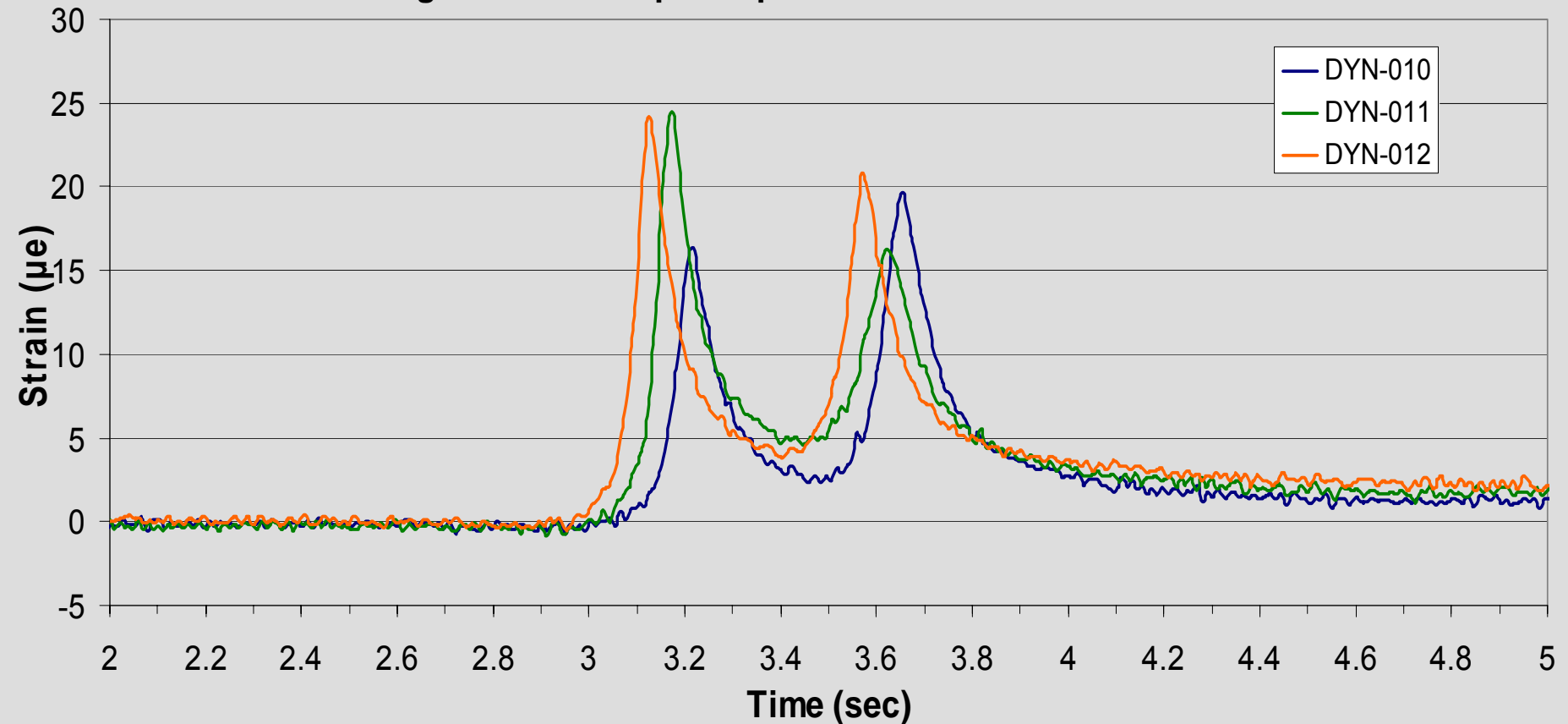
# AC CVL Test, July 2006

Longitudinal Strain in Intermediate Layer --  
Single Axle 20.5 kip 25 mph- AC 876B - Run 3 07/18/2006



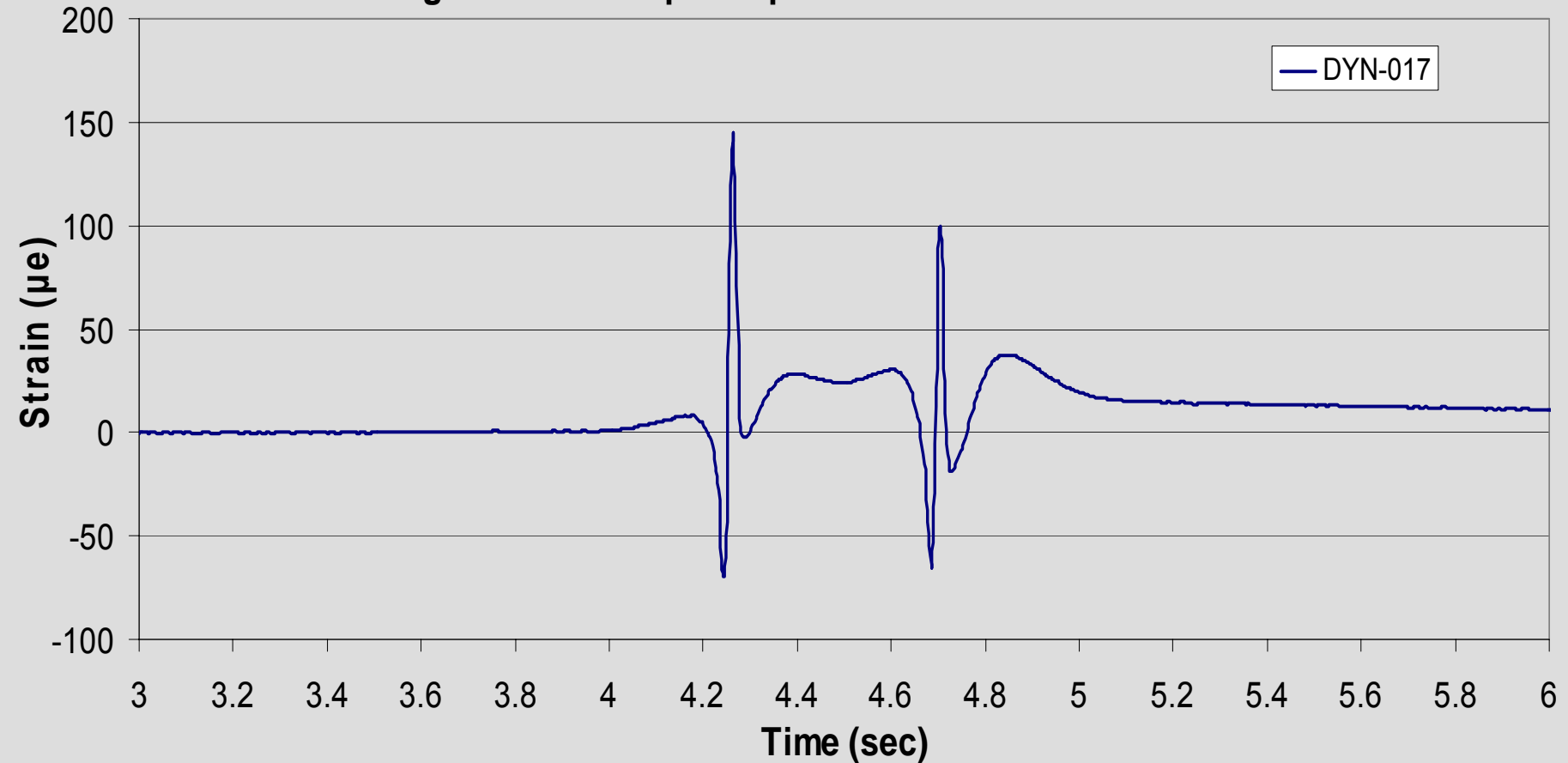
# AC CVL Test, July 2006

Transverse Strain in Intermediate Layer --  
Single Axle 20.5 kip 25 mph- AC 876B - Run 3 07/18/2006



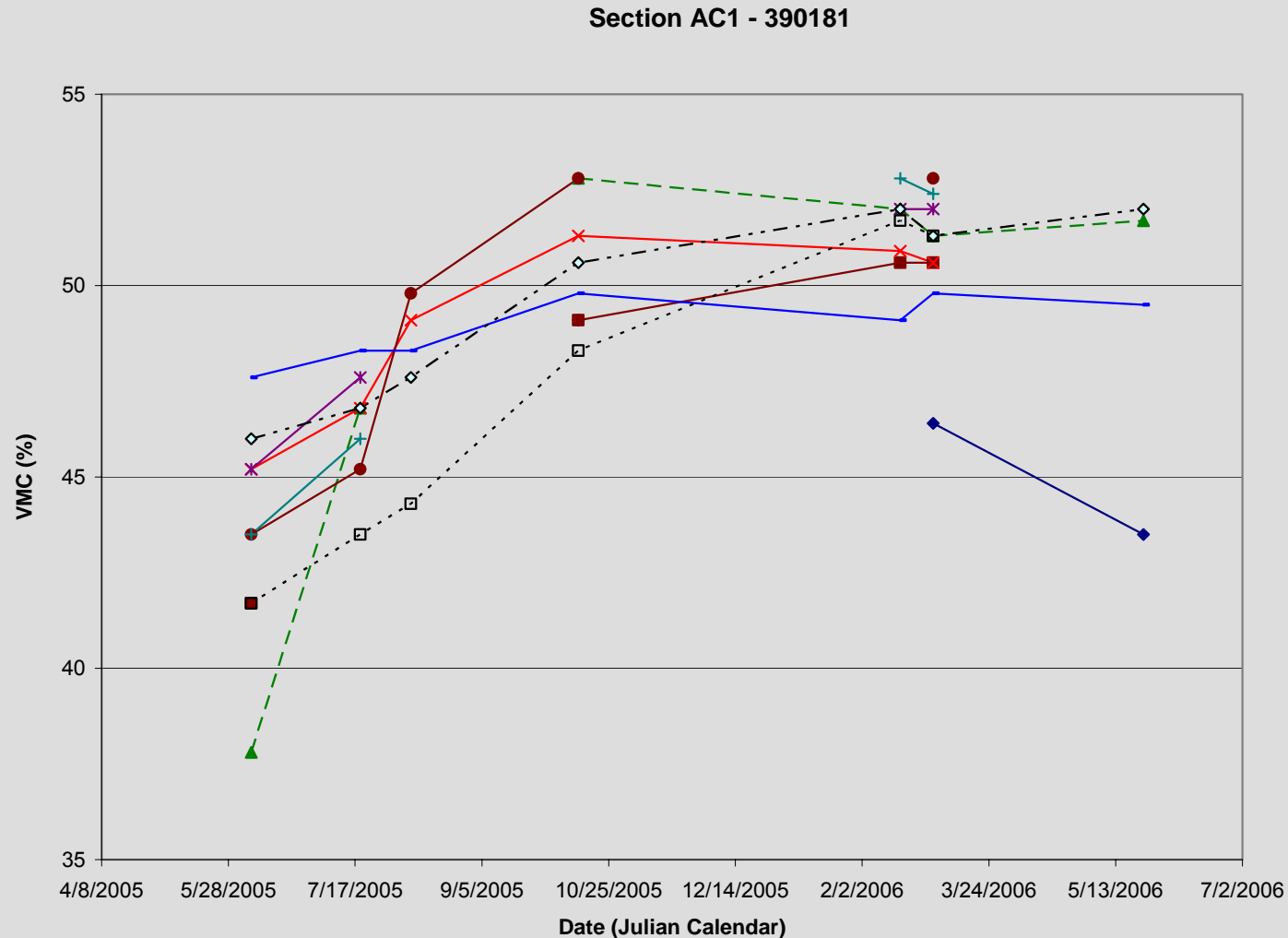
# AC CVL Test, July 2006

Longitudinal Strain in Surface Layer --  
Single Axle 20.5 kip 25 mph- AC 876B - Run 3 07/18/2006

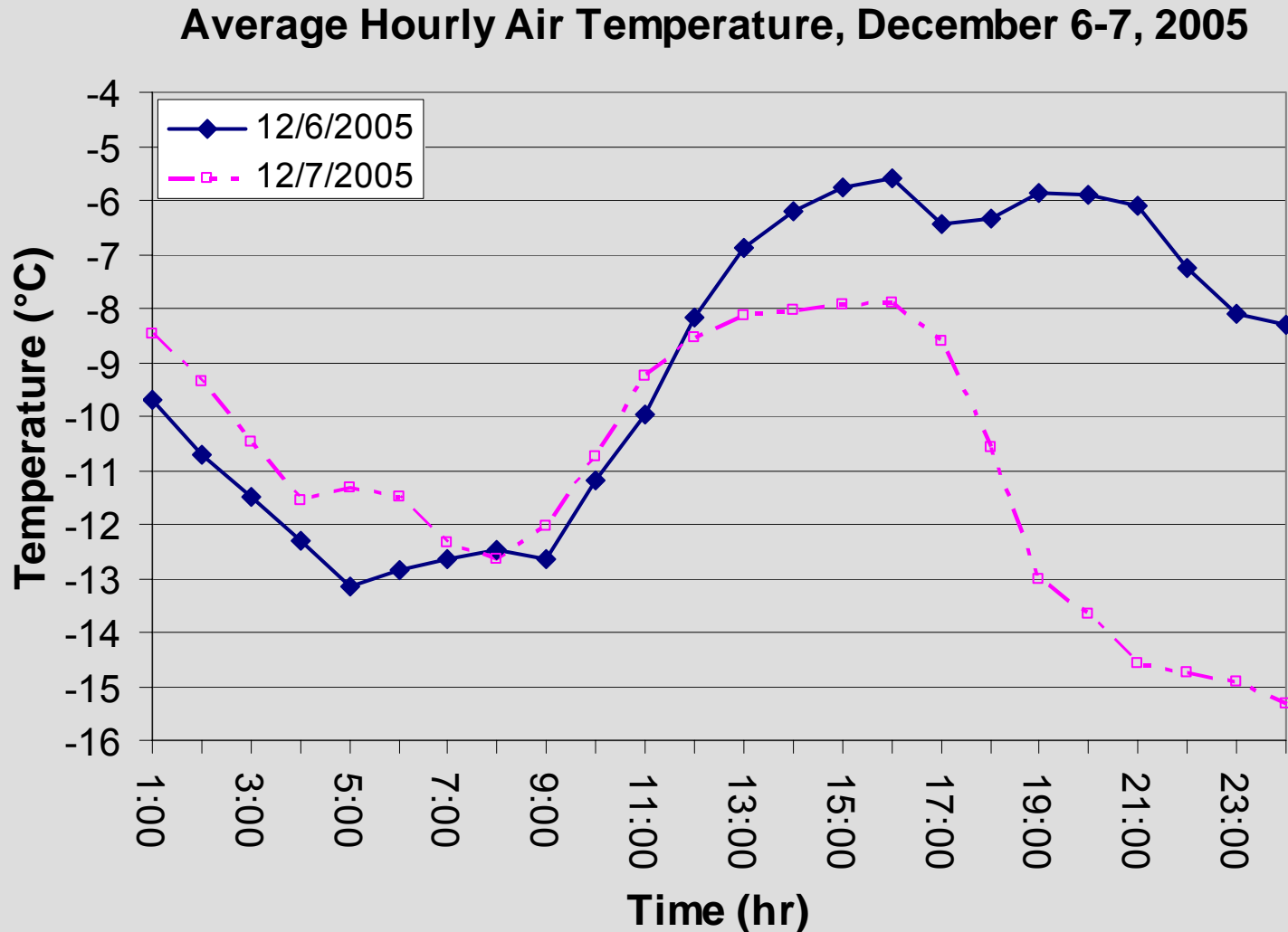


# VMC Variation – Section 876 (AC1 – 390181)

## 10 TDR Sensors



# Air Temperatures during CVL Test December 2005

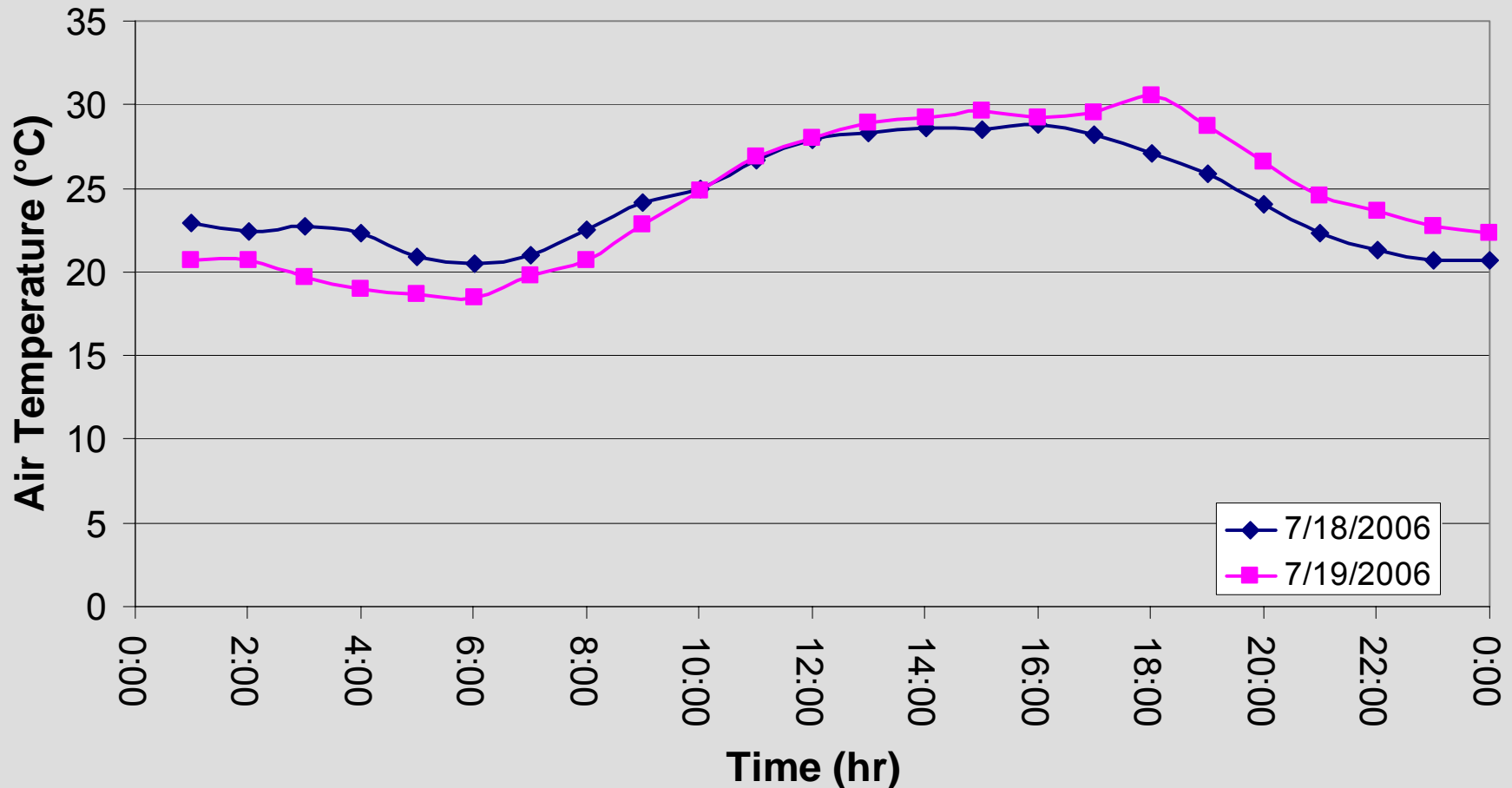




# Air Temperatures during CVL Test

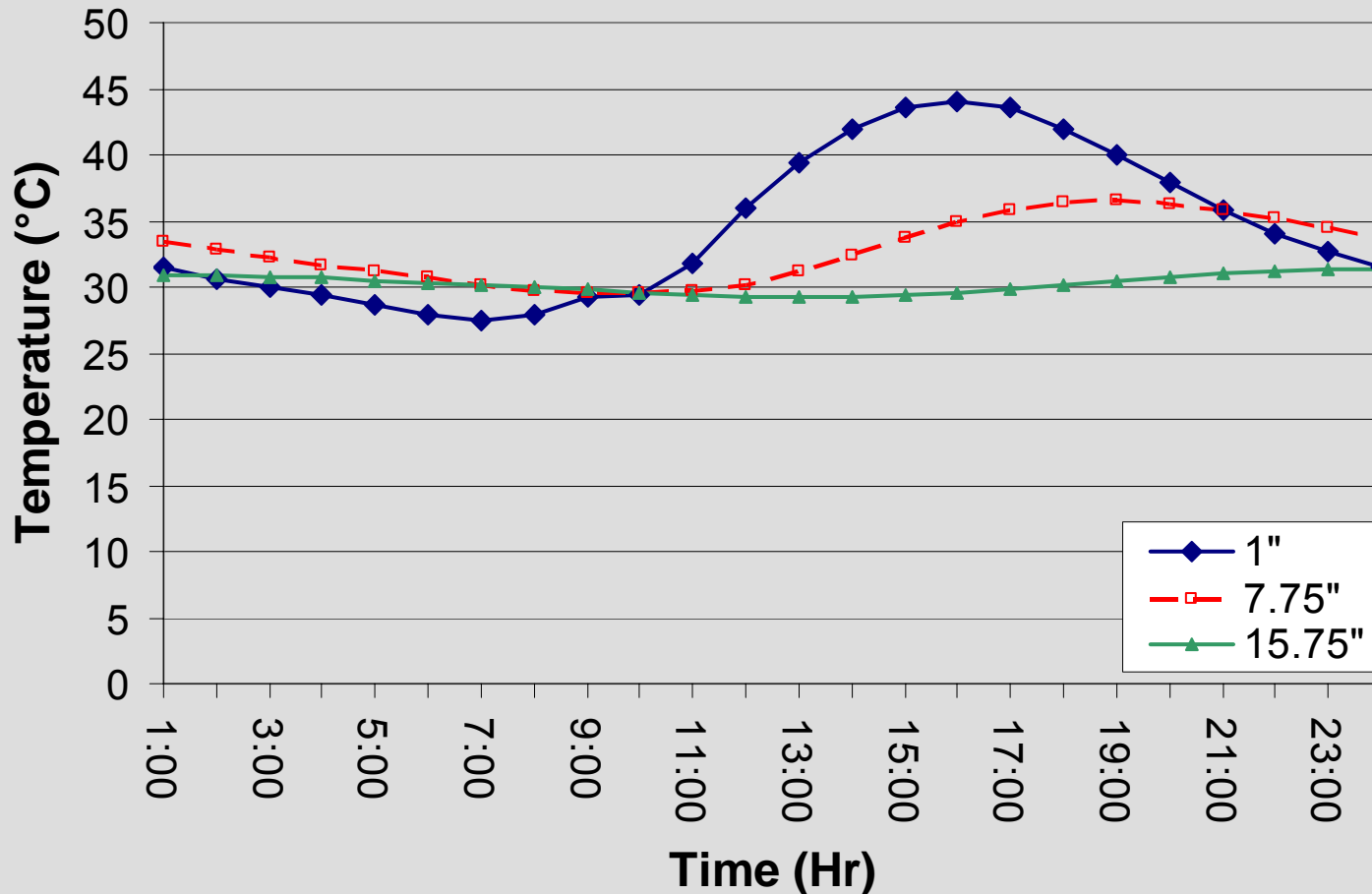
## July 2006

Average Hourly Air Temperature July 18-19, 2006



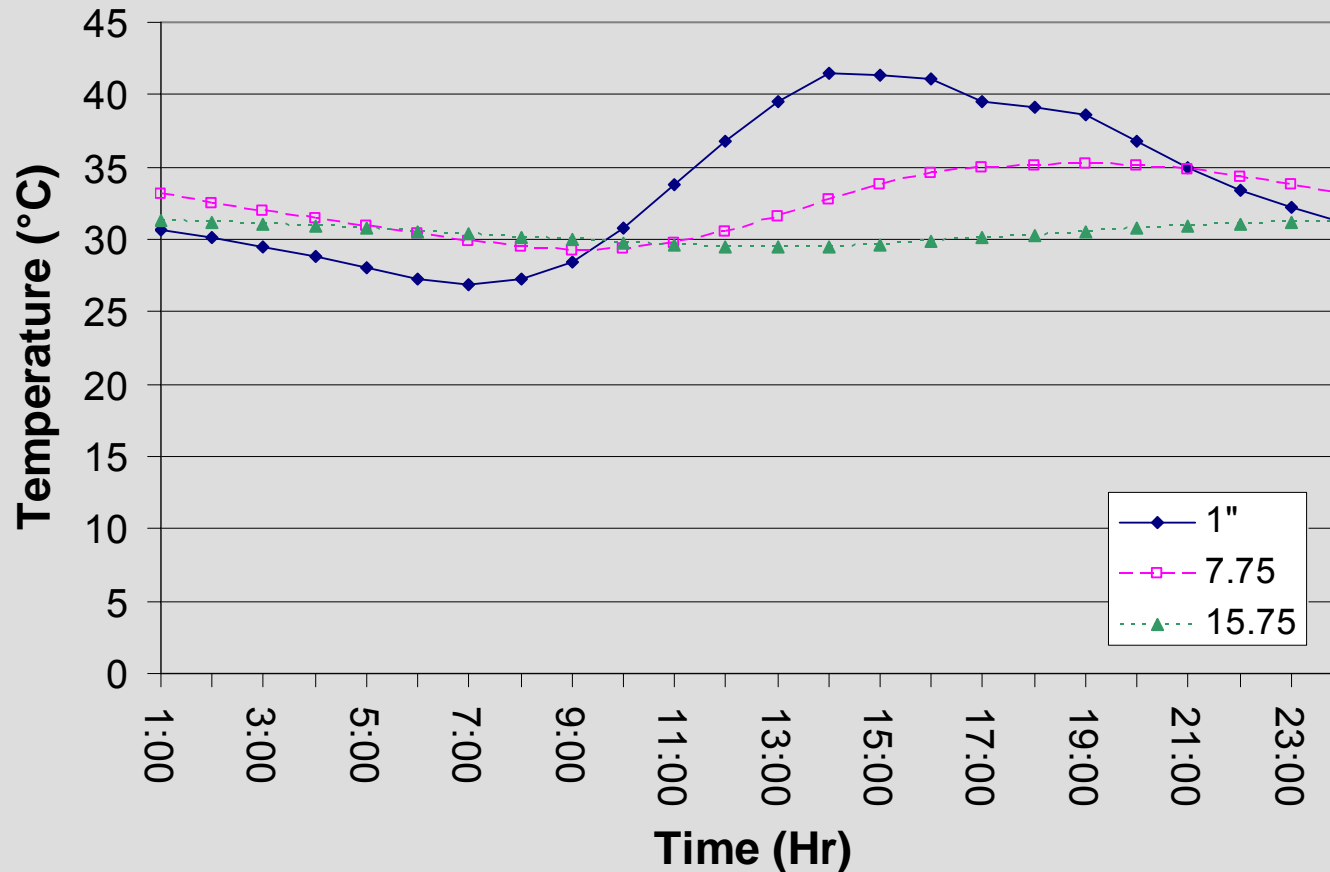
# Pavement temperatures during CVL Test July 18, 2006

## Pavement Temperature July 18, 2006



# Pavement temperatures during CVL Test July 19, 2006

## Pavement Temperature July 19, 2006



# Conclusions

## Fatigue Resistance Layer

- During December 2005 CVL test, longitudinal strain on FRL remained  $\leq 35\mu\epsilon$ , even at slowest speed
- During July tests at highway speeds of 45 mph and 55 mph, the strain in the FRL remained close to the design value under even the heaviest loads
  - In everyday use, such high-load strains will be rare
  - High-load strains at slower speeds will be even more rare (during traffic stoppage or slowdowns), though these did exceed design strain

# Conclusions

## Intermediate Layer and Subgrade

- Strains at bottom of intermediate layer are lower than at bottom of FRL, as expected.
- Maximum longitudinal strains are slightly higher than maximum transverse strains for all December runs and all single axle runs in July.
- Maximum subgrade observed pressure during CVL tests was 6.5 psi at 45 mph under 40 kip tandem axle load.



<http://webce.ent.ohiou.edu>

[www.ohio.edu/engineering](http://www.ohio.edu/engineering)



**OHIO**  
UNIVERSITY

# Pavement Analysis Program

## Principal Characteristics

- Materials are considered
  - homogeneous
  - isotropic
  - follow a linear stress-strain relationship
  - modulus of elasticity is same for compression and tension.
- All layers are
  - horizontal
  - have different specific elastic modulus and Poisson's Ratio
  - weightless
  - extend to infinity in the horizontal direction.
  - bottom layer also extends to infinity in the horizontal direction, but it is semi-infinite in the vertical direction.
- Stresses and displacements are zero at infinite depth within the semi-infinite bottom layer.

# Pavement Analysis Program

## Principal Characteristics (ctd)

- The top layer is free from shear stresses at the surface
- The load is applied at the surface of the top layer
  - distributed in a circular pattern
  - constant throughout the area
  - No normal stresses exist outside of the circular area.
- The layers are in continuous contact
- The layer interfaces are rough
- The layers act similarly to a composite medium.
- Both the horizontal and vertical displacements and the normal and shear stresses are the same very close to the interface of either one of the two layers.



# Pavement Analysis Program Inputs

- vertical displacement
- Stresses and strains:
  - vertical
  - horizontal
  - shear
  - Both stresses and strains are parallel to the three orthogonal axes.

# Analysis based on field core testing

## REAR DUAL WHEEL AC664 Dec'05 Averages and Calculated

| RUN | speed | S2-S6      | Calcul | S7,9,11 | Calcul | S8,10,11 | Calcul | LV1&4   | Calcul | LV2&3                                  | Calcul  | P1&P2 | Calcul |
|-----|-------|------------|--------|---------|--------|----------|--------|---------|--------|--|---------|-------|--------|
|     | mph   | ue         | ue     | ue      | ue     | ue       | ue     | in      | in     | in                                     | in      | psi   | psi    |
| 2   | 5     | 26.44      | 21.48  | 16.70   | 9.97   | 10.80    | 8.15   | 0.0053  | 0.0128 | 0.0017                                 | 0.00049 | 4.336 | 0.594  |
| 6   | 30    | 25.12      | 22.35  | 15.97   | 10.36  | 10.43    | 8.52   | 0.0048  | 0.0134 | 0.0014                                 | 0.00047 | 4.784 | 0.619  |
| 12  | 45    | 25.30      | 22.18  | 15.23   | 10.30  | 10.30    | 8.57   | 0.0035  | 0.0132 | 0.0012                                 | 0.00050 | 4.694 | 0.606  |
| 22  | 60    | 25.04      | 22.16  | 15.37   | 10.33  | 10.50    | 8.55   | 0.0041  | 0.0133 | 0.0014                                 | 0.00049 | 5.454 | 0.611  |
|     |       | @          | 16.25  | @       | 12.25  | @        | 12.25  | Surface |        | D <sub>surf</sub> - D <sub>22.25</sub> |         |       |        |
|     |       | Longit     |        | Longit  |        | Transv   |        |         |        |  |         |       |        |
|     |       | Bottom FRL |        | Bottom  | 302    | Bottom   | 302    |         |        |  |         |       |        |

## REAR DUAL WHEELS AC664 July'06 Average and Calculated

| RUN | Speed | S1-S6      | Calcul | S7,9,11 | Calcul | S10,12 | Calcul | LV1&4   | Calcul  | LV2&3                                  | Calcul  | P1&P2 | Calcul |
|-----|-------|------------|--------|---------|--------|--------|--------|---------|---------|--|---------|-------|--------|
|     | mph   | ue         | ue     | ue      | ue     | ue     | ue     | in      | in      | in                                     | in      | psi   | psi    |
| 47  | 5     | 118.73     | 68.96  | 72.93   | 29.16  | 64.20  | 20.59  | 0.0116  | 0.01784 | 0.0052                                 | 0.00097 | 4.419 | 1.219  |
| 55  | 25    | 86.80      | 68.72  | 51.57   | 29.18  | 40.30  | 22.27  | 0.0128  | 0.02005 | 0.0062                                 | 0.00278 | 4.715 | 1.297  |
| 61  | 45    | 77.27      | 69.48  | 43.33   | 29.20  | 40.50  | 20.95  | 0.0084  | 0.01852 | 0.0041                                 | 0.00133 | 4.025 | 1.267  |
| 69  | 55    | 70.63      | 70.27  | 37.90   | 29.17  | 35.95  | 20.88  | 0.0074  | 0.01866 | 0.0035                                 | 0.00137 | 4.305 | 1.282  |
|     |       | @          | 16.25  | @       | 12.25  | @      | 12.25  | Surface |         | D <sub>surf</sub> - D <sub>22.25</sub> |         |       |        |
|     |       | Longit     |        | Longit  |        | Transv |        |         |         |  |         |       |        |
|     |       | Bottom FRL |        | Bottom  | 302    | Bottom | 302    |         |         |  |         |       |        |

# Analysis based on laboratory sample testing

## REAR DUAL WHEEL AC664 Dec'05 Averages and Calculated

| RUN | speed | S2-S6      | Calcul | S7,9,11    | Calcul | S8,10,11   | Calcul | LV1&4   | Calcul | LV2&3                                  | Calcul  | P1&P2 | Calcul |
|-----|-------|------------|--------|------------|--------|------------|--------|---------|--------|--|---------|-------|--------|
|     | mph   | ue         | ue     | ue         | ue     | ue         | ue     | in      | in     | in                                     | in      | psi   | psi    |
| 2   | 5     | 26.44      | 13.30  | 16.70      | 5.92   | 10.80      | 4.97   | 0.0053  | 0.0100 | 0.0017                                 | 0.00030 | 4.336 | 0.418  |
| 6   | 30    | 25.12      | 13.94  | 15.97      | 6.17   | 10.43      | 5.23   | 0.0048  | 0.0107 | 0.0014                                 | 0.00029 | 4.784 | 0.449  |
| 12  | 45    | 25.30      | 13.75  | 15.23      | 6.10   | 10.30      | 5.21   | 0.0035  | 0.0104 | 0.0012                                 | 0.00030 | 4.694 | 0.435  |
| 22  | 60    | 25.04      | 13.84  | 15.37      | 6.13   | 10.50      | 5.22   | 0.0041  | 0.0106 | 0.0014                                 | 0.00030 | 5.454 | 0.441  |
|     |       | @          | 16.25  | @          | 12.25  | @          | 12.25  | Surface |        | D <sub>surf</sub> - D <sub>22.25</sub> |         |       |        |
|     |       | Longit     |        | Longit     |        | Transv     |        |         |        |  |         |       |        |
|     |       | Bottom FRL |        | Bottom 302 |        | Bottom 302 |        |         |        |  |         |       |        |

## REAR DUAL WHEELS AC664 July'06 Average and Calculated

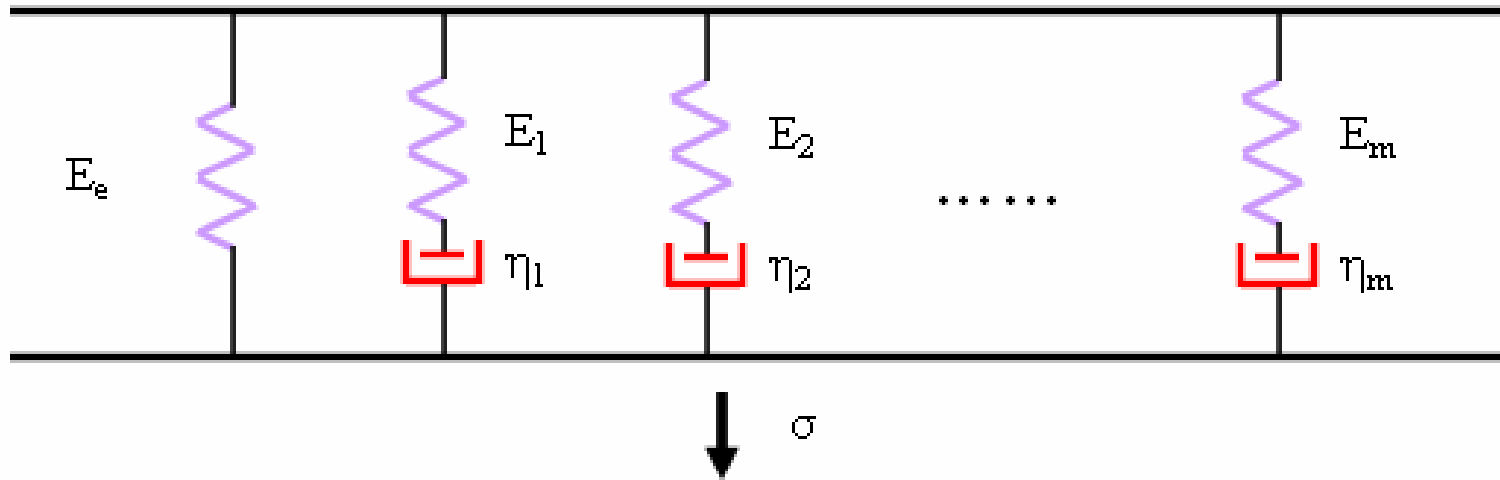
| RUN | Speed | S1-S6      | Calcul | S7,9,11    | Calcul | S10,12     | Calcul | LV1&4   | Calcul  | LV2&3                                  | Calcul  | P1&P2 | Calcul |
|-----|-------|------------|--------|------------|--------|------------|--------|---------|---------|--|---------|-------|--------|
|     | mph   | ue         | ue     | ue         | ue     | ue         | ue     | in      | in      | in                                     | in      | psi   | psi    |
| 47  | 5     | 118.73     | 38.26  | 72.93      | 15.20  | 64.20      | 11.33  | 0.0116  | 0.01484 | 0.0052                                 | 0.00055 | 4.419 | 0.844  |
| 55  | 25    | 86.80      | 39.31  | 51.57      | 15.67  | 40.30      | 12.51  | 0.0128  | 0.01539 | 0.0062                                 | 0.00143 | 4.715 | 0.901  |
| 61  | 45    | 77.27      | 39.02  | 43.33      | 15.42  | 40.50      | 11.68  | 0.0084  | 0.01503 | 0.0041                                 | 0.00073 | 4.025 | 0.881  |
| 69  | 55    | 70.63      | 39.43  | 37.90      | 15.39  | 35.95      | 11.64  | 0.0074  | 0.01514 | 0.0035                                 | 0.00075 | 4.305 | 0.891  |
|     |       | @          | 16.25  | @          | 12.25  | @          | 12.25  | Surface |         | D <sub>surf</sub> - D <sub>22.25</sub> |         |       |        |
|     |       | Longit     |        | Longit     |        | Transv     |        |         |         |  |         |       |        |
|     |       | Bottom FRL |        | Bottom 302 |        | Bottom 302 |        |         |         |  |         |       |        |

# Analysis based on laboratory sample testing sigmoidal equation

| REAR DUAL WHEEL |       |            |        | AC664   |        | Dec'05   |        | Averages |        | and                                    |         | Calculated |        |
|-----------------|-------|------------|--------|---------|--------|----------|--------|----------|--------|--|---------|------------|--------|
| RUN             | speed | S2-S6      | Calcul | S7,9,11 | Calcul | S8,10,12 | Calcul | LV1&4    | Calcul | LV2&3                                  | Calcul  | P1&P2      | Calcul |
|                 | mph   | ue         | ue     | ue      | ue     | ue       | ue     | in       | in     | in                                     | in      | psi        | psi    |
| 2               | 5     | 26.44      | 19.12  | 16.70   | 8.17   | 10.80    | 6.76   | 0.0053   | 0.0123 | 0.0017                                 | 0.00040 | 4.336      | 0.558  |
| 6               | 30    | 25.12      | 18.86  | 15.97   | 8.17   | 10.43    | 6.81   | 0.0048   | 0.0125 | 0.0014                                 | 0.00041 | 4.784      | 0.560  |
| 12              | 45    | 25.30      | 18.42  | 15.23   | 8.04   | 10.30    | 6.78   | 0.0035   | 0.0121 | 0.0012                                 | 0.00042 | 4.694      | 0.540  |
| 22              | 60    | 25.04      | 18.35  | 15.37   | 8.02   | 10.50    | 6.74   | 0.0041   | 0.0122 | 0.0014                                 | 0.00041 | 5.454      | 0.542  |
|                 |       | @          | 16.25  | @       | 12.25  | @        | 12.25  |          |        |  |         |            |        |
|                 |       | Longit     |        | Longit  |        | Transv   |        | Surface  |        | D <sub>surf</sub> - D <sub>22.25</sub> |         |            |        |
|                 |       | Bottom FRL |        | Bottom  | 302    | Bottom   | 302    |          |        |  |         |            |        |

| REAR DUAL WHEELS |       |        |        | AC664   |        |        |        | July'06 |         | Average                                |         | and   |        | Calculated |  |
|------------------|-------|--------|--------|---------|--------|--------|--------|---------|---------|--|---------|-------|--------|------------|--|
| RUN              | Speed | S1-S6  | Calcul | S7,9,11 | Calcul | S10,12 | Calcul | LV1&4   | Calcul  | LV2&3                                  | Calcul  | P1&P2 | Calcul |            |  |
|                  | mph   | ue     | ue     | ue      | ue     | ue     | ue     | in      | in      | in                                     | in      | psi   | psi    |            |  |
| 47               | 5     | 118.73 | 47.51  | 72.93   | 20.15  | 64.20  | 14.81  | 0.0116  | 0.01574 | 0.0052                                 | 0.00067 | 4.419 | 0.948  |            |  |
| 55               | 25    | 86.80  | 37.65  | 51.57   | 15.72  | 40.30  | 12.61  | 0.0128  | 0.01472 | 0.0062                                 | 0.00118 | 4.715 | 0.859  |            |  |
| 61               | 45    | 77.27  | 34.12  | 43.33   | 14.04  | 40.50  | 10.81  | 0.0084  | 0.01408 | 0.0041                                 | 0.00060 | 4.025 | 0.794  |            |  |
| 69               | 55    | 70.63  | 33.45  | 37.90   | 13.60  | 35.95  | 10.49  | 0.0074  | 0.01401 | 0.0035                                 | 0.00060 | 4.305 | 0.787  |            |  |
|                  |       | @      | 16.25  | @       | 12.25  | @      | 12.25  |         |         |  |         |       |        |            |  |
|                  |       | Longit |        | Longit  |        | Transv |        | Surface |         | D <sub>surf</sub> - D <sub>22.25</sub> |         |       |        |            |  |
|                  |       | Bottom | FRL    | Bottom  | 302    | Bottom | 302    |         |         |  |         |       |        |            |  |

# Mechanical Model - The Generalized Maxwell model



$$E(t) = E_e + \sum_{i=1}^m E_i e^{-(t/\tau_i)}$$

# Material Properties

| Layer    | Instantaneous Elastic Modulus<br>Used in ABAQUS (ksi) | Measured Relaxation<br>Modulus (ksi) |
|----------|---|--------------------------------------|
| SMA      | 706   | 726.6                                |
| ODOT442  | 529   | 501.8                                |
| ODOT302  | 1118  | 1169.0                               |
| FRL      | 1176  | 1518.5                               |
| Base     | 20 <sup>\$</sup>                                      | 10 – 40* <sup>\$</sup>               |
| Subgrade | 8 <sup>\$</sup>                                       | 7.5 <sup>\$</sup>                    |

<sup>\$</sup> these are resilient modulus;

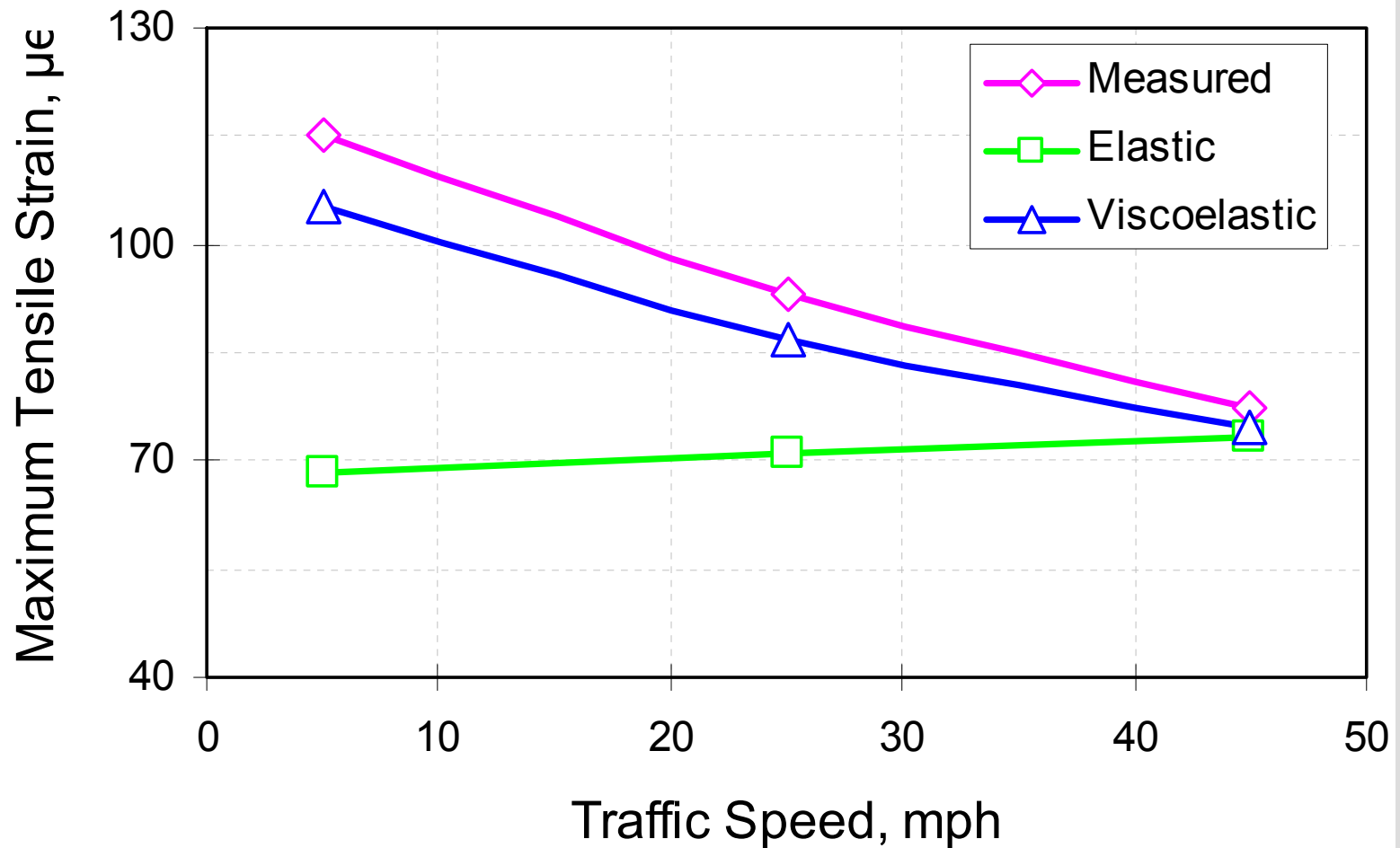
\*This is the normal range for aggregates;

All HMA moduli are referred at a temperature of 21.1 C.

# Elastic FE Model vs. Viscoelastic FE Model

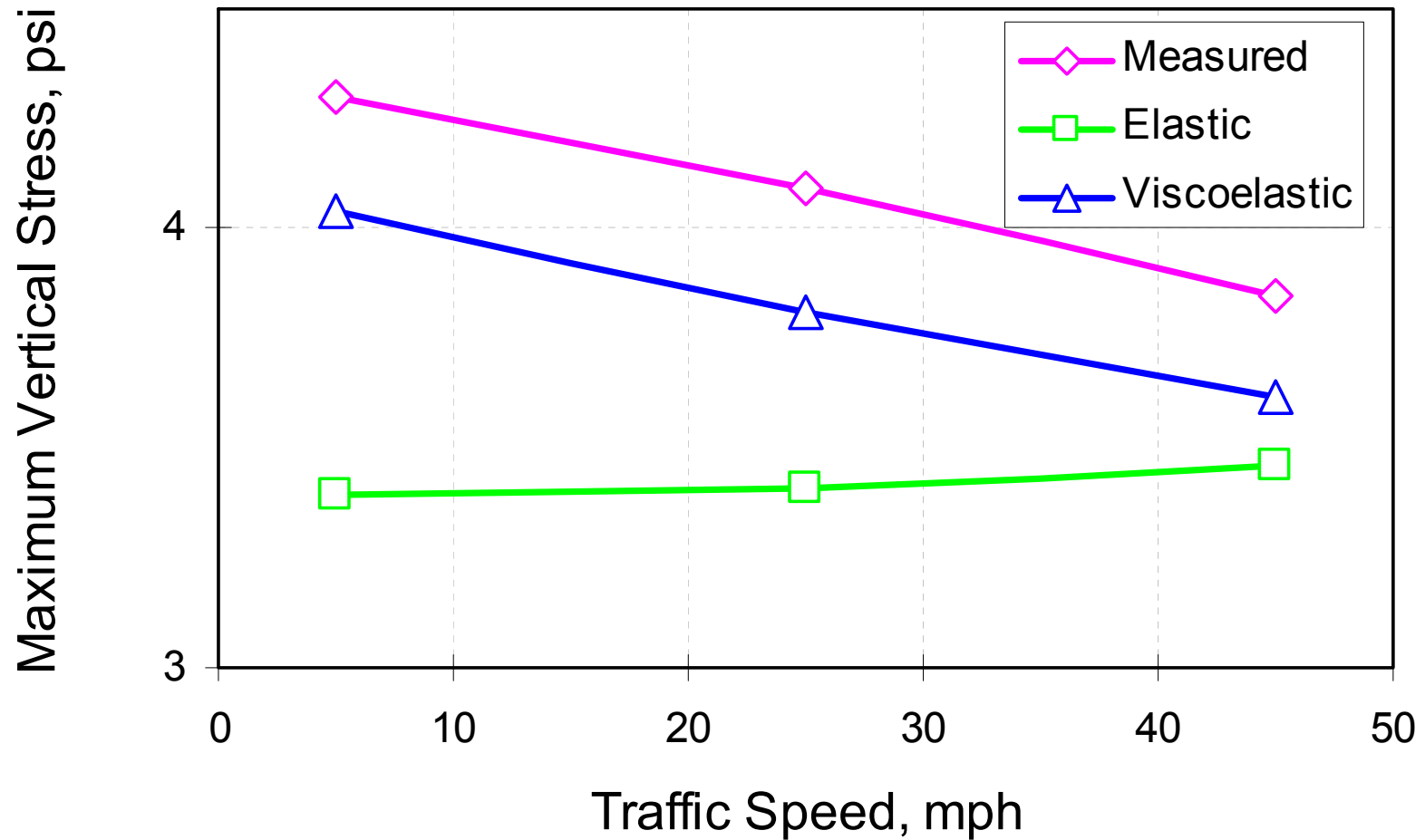
- To compare their relative performance in predicting pavement response at different truck speeds of 5 mph, 25 mph, and 45 mph.
- Pavement response was collected at the U.S. 30 test section.
- In the elastic FE model, the effect of pavement temperature is included.
- Both models are calibrated to pavement response at a truck speed of 55 mph.
- It is noted that pavement temperature slightly decreased when truck speed decreased from 45 mph to 5 mph.

# Elastic FE Model vs. Viscoelastic FE Model

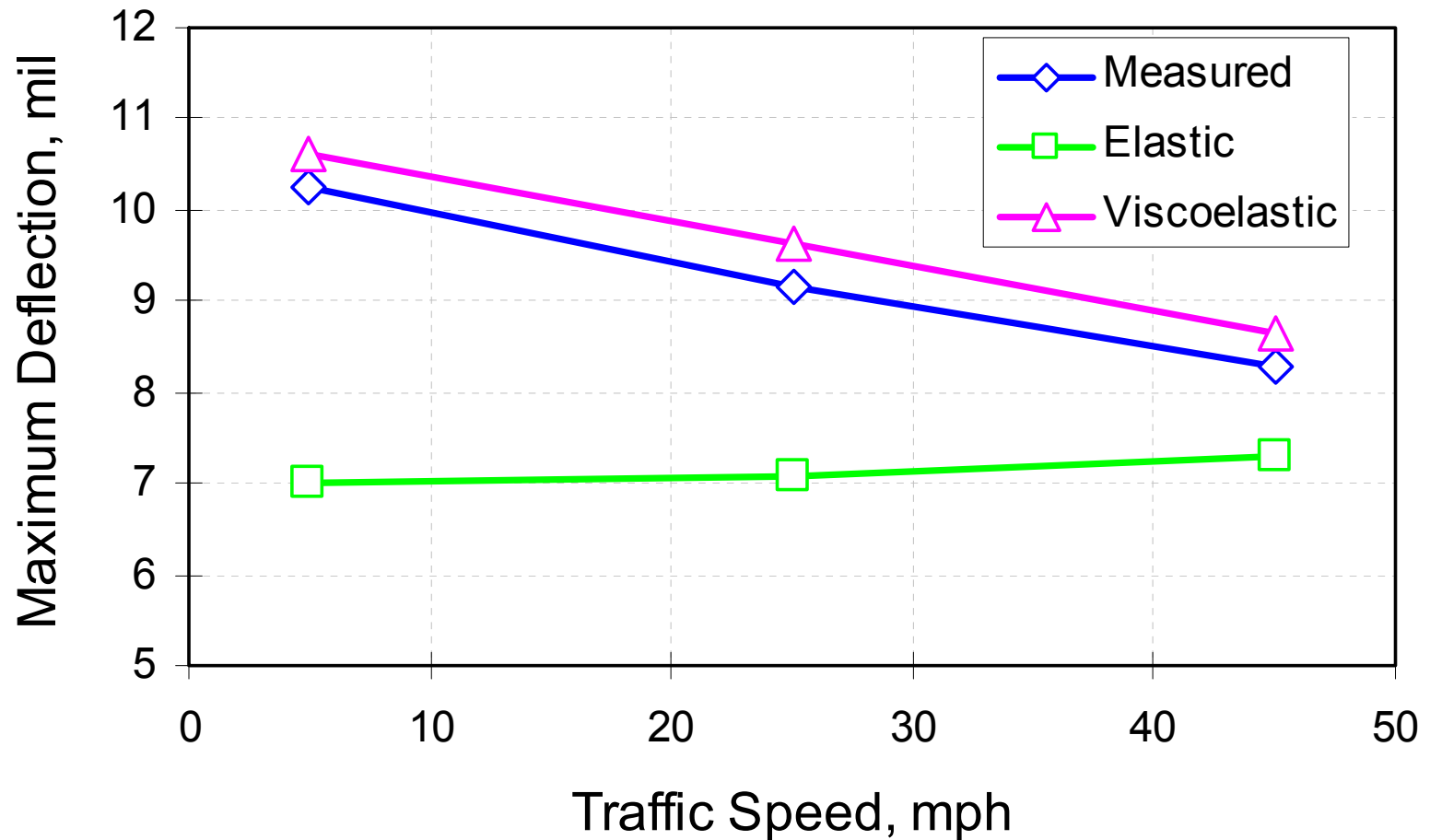




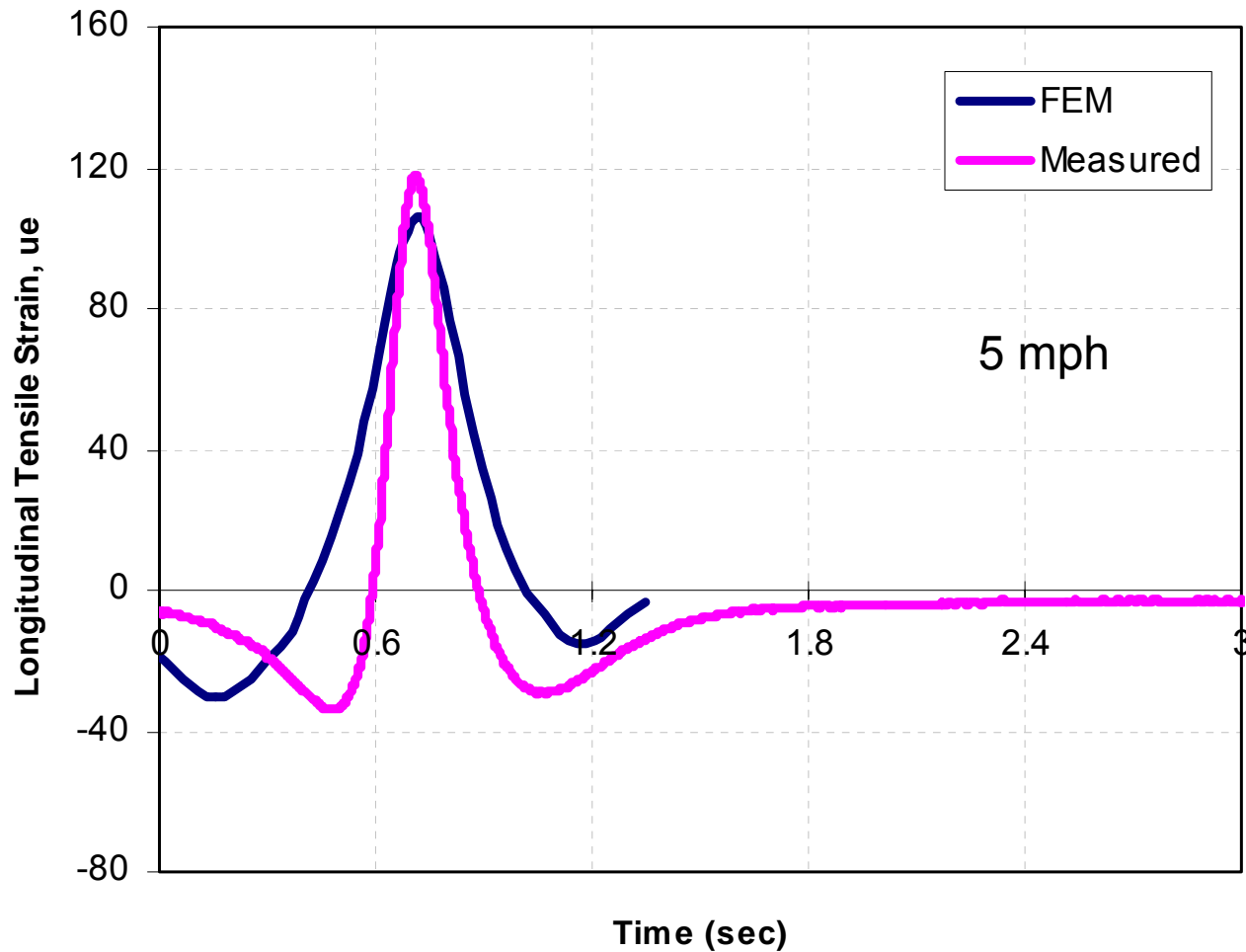
# Elastic FE Model vs. Viscoelastic FE Model



# Elastic FE Model vs. Viscoelastic FE Model



# Comparison of Longitudinal Tensile Strain



# Conclusions

## Elastic Layer Analysis

- General agreement between computed and measured values of longitudinal strain at bottom of FRL only when using resilient modulus from field cores, and only at higher speeds.
- Calculated longitudinal and transverse strains at bottom of intermediate layer are are always lower than measured values.
- Calculated surface deflections are always higher than measured values.
- Both the calculated net pavement deflection and the subgrade pressure are lower than the measured values.

# Conclusions

## Elastic Layer Analysis

- Using dynamic modulus of laboratory-prepared specimens with sigmoidal equation does not yield reasonably close verification of any parameters.
- Using resilient modulus of laboratory-prepared specimens does not yield reasonably close verification of any parameters.
- Using resilient modulus of field cores generally yields correct trends, though not values matching measurements.
- ELS theory is capable of matching one parameter but not all.
- ELS not appropriate for simulating time-dependent loading due to trucks.
- Some discrepancies may arise from differences in air void content and density between field cores and laboratory prepared samples.



<http://webce.ent.ohiou.edu>

[www.ohio.edu/engineering](http://www.ohio.edu/engineering)



**OHIO**  
UNIVERSITY